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Precise Frequency and Period Measurements for Slow Slew Rate Signals Based on the Modified Method of the Dependent Count

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Abstract: This paper describes an application of novel modified method of the dependent count for measuring the frequency (period) of slow slew rate signals (common for the conversion-to-digital of resistance, capacitance, inductance or resistive-sensor-bridge signals based on direct connection to a microcontroller). The AVR 8-bit ATmega168-20PI microcontroller (Atmel), based on advanced reduced instruction set computing architecture, was used. The modified method of the dependent count improves the accuracy of period measurements for the slow slew rate signals of triangular, sine, exponential rise and fall, as well as rectangular waveforms, by 2-to-3 orders in comparison with the accuracy achieved with classical indirect counting in all frequency ranges. The error is evaluated from the statistical characteristics and histograms of measured pulse periods, quantitatively confirming the advantages of the modified method for frequency (period) measurements for non-square pulse signals. Measurements are further improved (becoming about 1.5 times more accurate) for some waveforms when an external Schmitt trigger is used. *Copyright © 2009 IFSA.*

Keywords: Period measurement; Modified method of the dependent count; Frequency measurement

1. Introduction

Frequency and period of non-rectangular waveform signals that have a slow slew rate - such as triangular, sine, exponential rise and fall waveform signals - must often be measured. Low frequency measurements (50, 100 and 200 Hz) involving signals with a slow slew rate are common, for example, in the conversion-to-digital of resistance, capacitance, inductance or resistive-sensor-bridge signals based on direct connection to a microcontroller [1, 2]. Such an approach offers a simple low-cost interface

between microcontrollers with embedded timer/counter and quasi-digital sensors with a period, time interval or frequency output. The indirect (period) counting method for slow slew rate signals is susceptible to errors because of changes in the input trigger threshold due to several external and internal noise sources. In addition to thermal noise, there are other trigger noise sources that are program dependent [3] or result from interference in the microcontroller power supply [4, 5]. Very often, trigger errors predominate over the inherent quantization error, so that precise frequency or period measurements require the use of an external input signal-forming device, such as an amplifier-limiter with a Schmitt trigger circuit, which yields rectangular waveform impulses from the slow slew rate signal [3]. However, that solution increases the hardware cost and reduces reliability, because the probability of failure is directly proportional to the number of components being used.

Fig. 1 shows a triangular signal whose period is determined by measuring the time interval between consecutive voltage crossings of its leading ramp. In a noiseless system (V_{th} undistorted), the period measured would be T_x and the input trigger points would be at S_1 and S_2 . However, noise and interference added to V_{th} shift the trigger points, so that the measured period will be $T_x + \tau_1 + \tau_2$. Usually, $\tau_1 \neq \tau_2$ because $\Delta V_1 \neq \Delta V_2$.

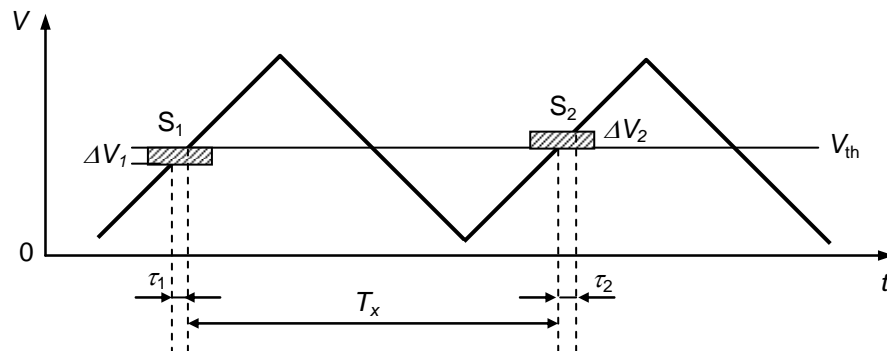


Fig. 1. Error level related to trigger point uncertainty when measuring the period of a triangular signal.

Frequency-to-digital conversions are immune to that error component, because it is not necessary to extract a separate period from the pulse train and $\tau_1 = \tau_2 = 0$, so that we can measure f_x and then calculate the period as $T_x = 1/f_x$ [6]. But the standard direct counting method for frequency measurement applied to low frequencies has either a very high quantization error or a long measurement time. For example, in order to have a quantization error below 0.01% at $f_x = 100$ Hz, the conversion time must be larger than 100 s. Advanced methods for frequency measurement, such as ratiometric, reciprocal, M/T, constant elapsed time (CET), single- and double-buffered or direct memory access (DMA) methods, and methods using a non-redundant reference frequency [6] all have a constant quantization error regardless of signal frequency; however, their conversion time is redundant, which increases the dynamic error and the measurement time for all frequencies except the nominal one. It would be preferable to use an alternative method related to frequency (period) conversion, one that would have a constant quantization error over the entire frequency range measured and a non-redundant conversion time.

This paper describes the application of a novel approach to the measurement of slow slew rate signal frequency (period) based on a modification of method of the dependent count; this approach uses the common modern AVR 8-bit ATmega168 microcontroller (*Atmel*), which is based on advanced reduced instruction set computing (RISC) architecture. The main advantages of the microcontroller-based method are the use of the least possible amount of hardware, high reliability and low price. All these factors are very important for applications where resistive, capacitive, inductive or resistive bridge sensing elements are directly interfaced to standard microcontrollers in order to convert appropriate parameters into digital information.

2. Novel Modified Method of the Dependent Count

The modified method of the dependent count combines the advantages of classical and advanced methods and ensures a constant relative quantization error over an entire frequency range and also high speed due to non-redundant conversion time. The time diagram of the modified method of the dependent count is shown in Fig. 2.

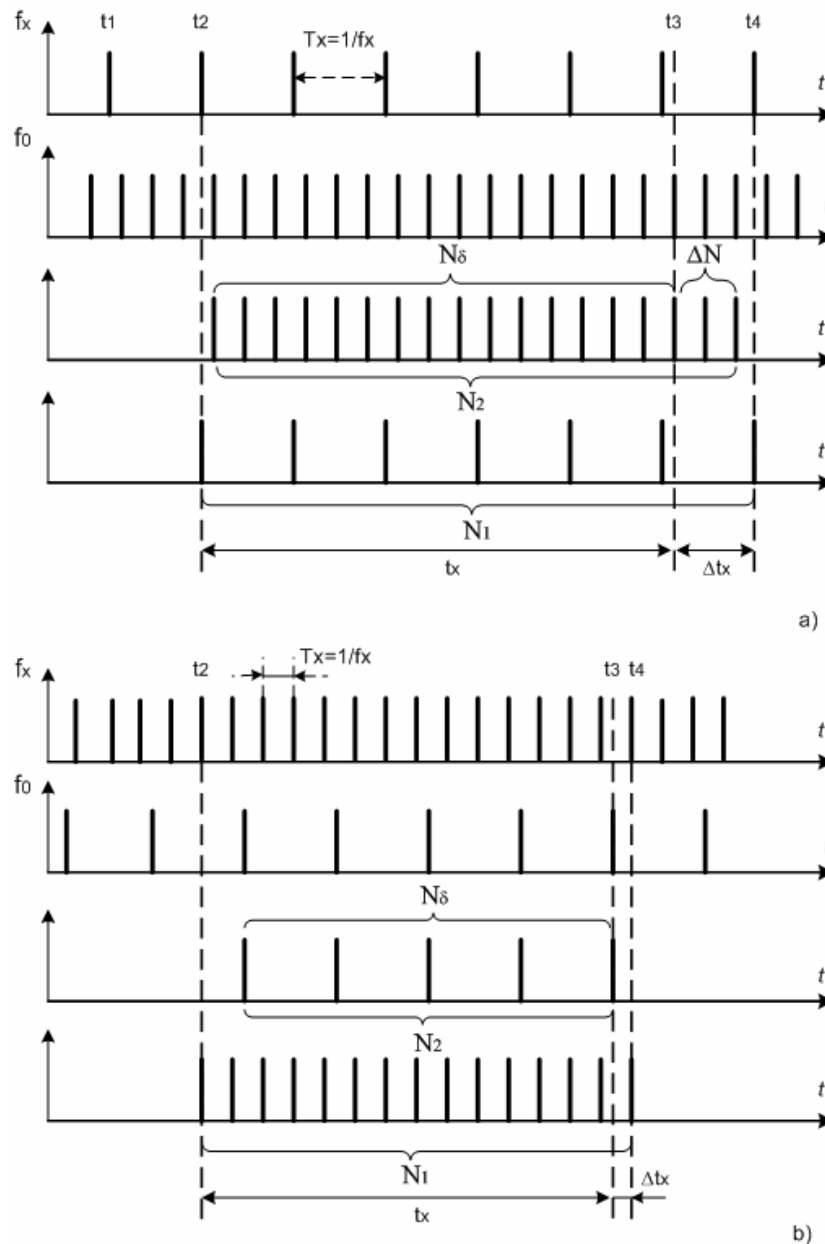


Fig. 2. Time diagrams of the modified method of the dependent count in cases of $f_x < f_0$ (a) and $f_x > f_0$ (b).

Let us consider two possible cases. In the case of $f_x < f_0$, where f_0 is the reference frequency, time diagrams of the method are similar to the previously proposed method of the dependent count [7] but without the preliminary stage for frequency comparison ($f_x > f_0$). In other words, a measurement will start at the t_2 moment: thus, beginning from moment t_2 according to the modified method, pulses of both frequencies f_x and f_0 are counted (the numbers N_1 and N_2 respectively). The count continues during the

time interval between t_2 and t_4 . The reference gate time between t_2 and t_3 is equal to the integer value for the period of the reference frequency f_0 and is determined by the number $N_\delta = 1/\delta$, where δ is the relative error of measurement. The necessary relative error can be chosen at the beginning of each measurement or set up for all measurements at once according to a measuring algorithm. The counts of both frequencies (f_x and f_0) are stopped by the next pulse after an unknown frequency f_x after moment t_3 . The number N_2 is the integer number of the period of the reference frequency f_0 :

$$N_2 = N_\delta + \Delta N, \quad (1)$$

where $\Delta N = (0 \div \Delta N_{max})$ is the additional value of the period of the reference frequency f_0 counted during the Δt time interval (between t_3 and t_4). In turn, N_1 is the integer value of pulses of unknown frequency f_x . The time of measurement T_{meas} is an integer value of converted periods of the signal with frequency f_x :

$$T_{meas} = T_x \cdot N_1 = \frac{N_1}{f_x} \quad (2)$$

This time interval can also be approximated as:

$$T_{meas} \cong T_0 \cdot N_2 = \frac{N_2}{f_0} = \frac{N_\delta + \Delta N}{f_0} = \left(\frac{1}{\delta} + \Delta N \right) \cdot T_0 \quad (3)$$

From equations (2) and (3) it follows that an unknown frequency f_x and period T_x should be calculated according to the following formulas:

$$f_x = \frac{N_1}{N_2} \cdot f_0 \quad \text{and} \quad T_x = \frac{N_2}{N_1 \cdot f_0}; \quad (4)$$

The quantization error for these measurements results from the fact that the time of measurement $T_{meas} = t_x + \Delta t_x$ is not equal to the integer number N_2 of the period of the reference frequency $T_0 = 1/f_0$:

$$T_{meas} \neq N_2 \cdot T_0 \neq \frac{N_2}{f_0} \quad (5)$$

A change of the frequency f_x between specific limits will change the interval T_{meas} , and the number of counted impulses N_2 will change from $\Delta N = 0$ to $\Delta N = \Delta N_{max}$, where ΔN_{max} is the number of impulses in the interval $\Delta t_{xmax} = T_x$. Taking into account that the period of these input impulses is T_x , we will have

$$\Delta N_{max} = \frac{T_x}{T_0} = \frac{f_0}{f_x} \quad (6)$$

The maximum quantization error will take place when the number of counted impulses N_2 is minimal and equal to N_δ . Then, the maximum relative error will be

$$\delta_{max} = \frac{1}{N_{min}} = \frac{1}{N_\delta} = \delta \quad (7)$$

Hence, the maximum error is determined only by N_δ and does not depend on the measured frequency. The minimum error will be at $N = N_{max}$. Since $N_{max} = N_\delta + \Delta N_{max}$,

$$\delta_{\min} = \frac{1}{N_{\delta} + \Delta N_{\max}} \quad (8)$$

Selecting a large $N_{\delta} = 1/\delta$ reduces the quantization error. The measurement time can be kept short by selecting a large reference frequency f_0 .

In the common case the mean-square quantization error will be

$$\sigma_q = \frac{1}{N_{\delta} \sqrt{6}} = \frac{\delta}{\sqrt{6}} \quad (9)$$

The coefficient of relative error change should be calculated according to the following equation:

$$\alpha = \delta_{\max}/\delta_{\min} = (N_{\delta} + \Delta N_{\max})/N_{\delta}. \quad (10)$$

Taking into account a wide frequency range of measurement, the time of measurement $T_{meas} = t_x + \Delta t_x$ should be calculated as

$$\begin{cases} T_{meas} = T_x, & \text{if } \frac{N_{\delta}}{f_0} < T_x \\ T_{meas} = \frac{N_{\delta}}{f_0} + (0 \div T_x), & \text{if } \frac{N_{\delta}}{f_0} \geq T_x \end{cases} \quad (11)$$

The resolution of method in the case of $f_x < f_0$ can be calculated according to the following equation:

$$Q_N = \frac{f_0 \cdot N_1}{N_2(N_2 + 1)} = \frac{f_x}{(N_2 + 1)} = \frac{f_x}{(N_{\delta} + \Delta N + 1)}. \quad (12)$$

For the case of $f_x > f_0$, time diagrams of the method are shown in Fig. 2b. N_2 is equal to N_{δ} ($\Delta N = 0$). Unknown frequency f_x , or period $T_x = 1/f_x$, should be calculated according to equations (4). The relative error $\delta = \delta_{\max} = \delta_{\min}$ and the coefficient of relative error change $\alpha = 1$. The time of measurement in this case will be

$$T_{meas} = \frac{N_{\delta}}{f_0} + (0 \div T_x). \quad (13)$$

The resolution of modified method of the dependent count in case of $f_x > f_0$ can be determined as

$$Q_N = \frac{f_x}{(N_{\delta} + 1)}. \quad (14)$$

In comparison with an earlier-proposed method of the dependent count [7], the new recently patented modified method has high programmable accuracy, scalable resolution, non-redundant time of measurement and a wide frequency range; additionally, it allows us to measure frequency that exceeds the reference frequency ($f_x \gg f_0$) without additional hardware or time for preliminary frequency estimation or comparison: ($f_x \gg f_0$). In order to measure $f_x < f_0$ or $f_x > f_0$, no additional decision-making procedure is necessary. The calculation is done automatically (see Fig. 2a and 2b respectively).

3. Measurement System Set-up

In order to experimentally validate the advantages of the modified method of the dependent count for frequency (period) measurements of slow slew rate signals with different waveforms, the common modern AVR 8-bit ATmega168-20PI (*Atmel*) microcontroller was used. Fig. 3 shows the measurement set-up.

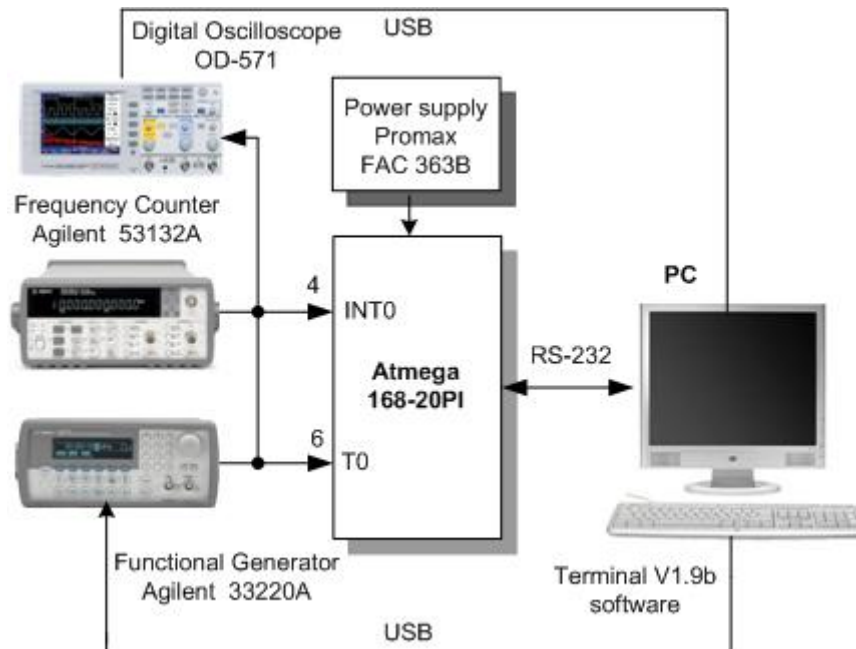
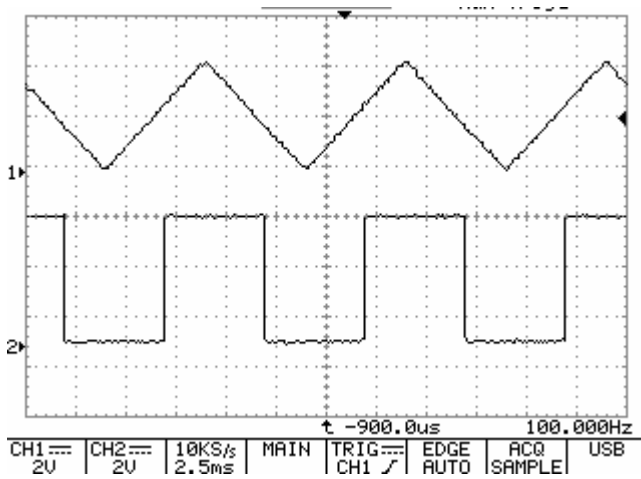


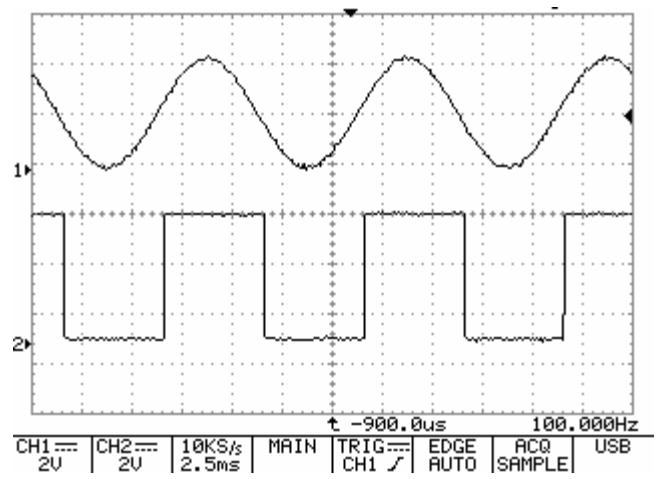
Fig.3. Measurement set-up to determine the period of signals having a slow slew rate.

Different waveform (rectangular, triangular, sine, exponential rise and exponential fall) signals whose periods were to be measured were fed from a function generator (Agilent 33220A) to inputs INT0 (external interrupt request 0, programmed to interrupt the main program when a rising edge crosses its voltage threshold), and T0 (Timer/Counter 0) of the ATmega168-20 PI microcontroller running on a 20 MHz clock. The microcontroller converted periods of slow slew rate signal to digital by using the modified method of the dependent count implemented by software relying only on the internal functional-logical architecture of the microcontroller. The internal reference frequency was $f_0 = 625$ kHz with the relative error $\delta_0 = \pm 0.0001$ %. The programmable relative error of period measurements was chosen as $\delta = \pm 0.0005$ %. The microcontroller was supplied at +5 V dc by a Promax FAC-363B power supply. The frequency generated by the Agilent 33120A was 100 Hz; its respective period was 10 ms and signals were monitored by a high precision calibrated frequency counter (Agilent 53132A). This frequency was chosen to be the same as in experiments described in [3, 4, 8-10] in order to compare the experimental results. Each slow slew rate signal was measured by the microcontroller directly as well as through an external Schmitt trigger integrated circuit 74HC14D (Fig. 4 a-e). The waveform signal parameters are shown in Table 1. The peak-to-peak amplitude was approximately 5 V. The Promax OD-571 oscilloscope monitored the signal waveforms.

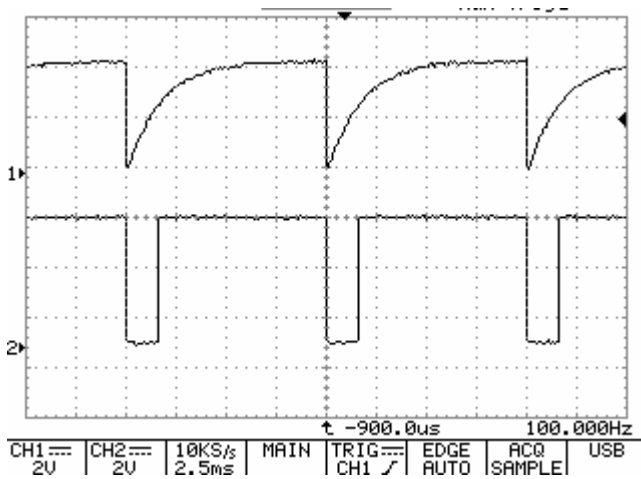
The measured period value was sent to a PC via an RS-232 interface implemented with the ST202D integrated circuit. The user interface was implemented with the help of terminal software (Terminal V1.9b for Windows) [11]. Period measurements were taken every second until a total of 60 measurements had been recorded. The measurement error was evaluated from histograms and appropriate statistical characteristics.



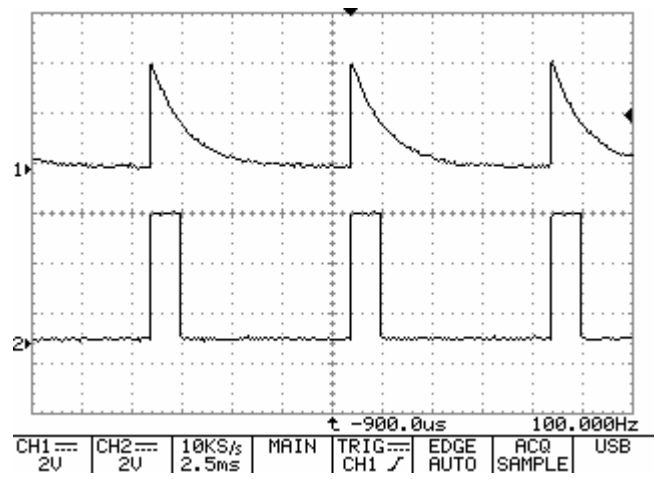
a)



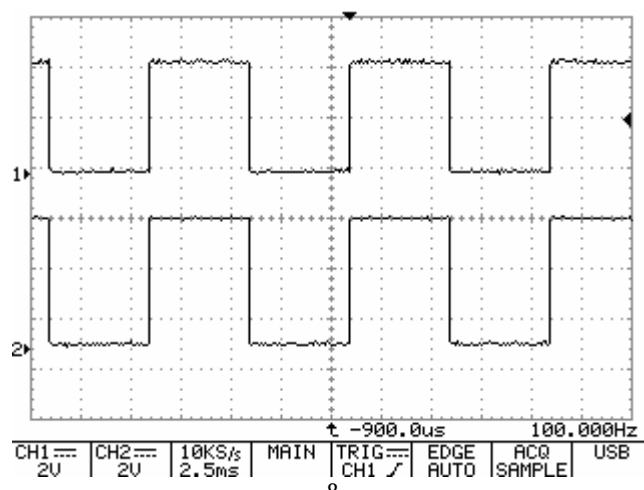
b)



c)



d)



e)

Fig. 4. Input forming device time diagrams: input (1) and output (2) signals for different investigated waveforms.

Table 1. The Waveform Signal Parameters.

	Triangular	Sine	Exponential Rise	Exponential Fall
Rise Time:				
1. Input Signal	3.275 ms	2.82 ms	3.733 ms	78.49 μ s
2. Schmitt Trigger Output	78.73 μ s	78.73 μ s	80.00 μ s	81.29 μ s
Fall Time				
1. Input Signal	3.3 ms	2.653 ms	75.47 μ s	3.273 ms
2. Schmitt Trigger Output	78.73 μ s	78.73 μ s	81.31 μ s	80.00 μ s

4. Experimental Results and Discussion

The measured periods and the probability densities for triangular waveform signals of 100 Hz with 50 % symmetry are shown in Fig. 5 (a, b). The statistical characteristics are shown in Table 2. The number of equidistant classes k in the probability density function chart for a sampling of 60 measurements was calculated according to [12] and is $k = 5$. The relative error can be reduced 1.53 times by using an external Schmitt trigger.

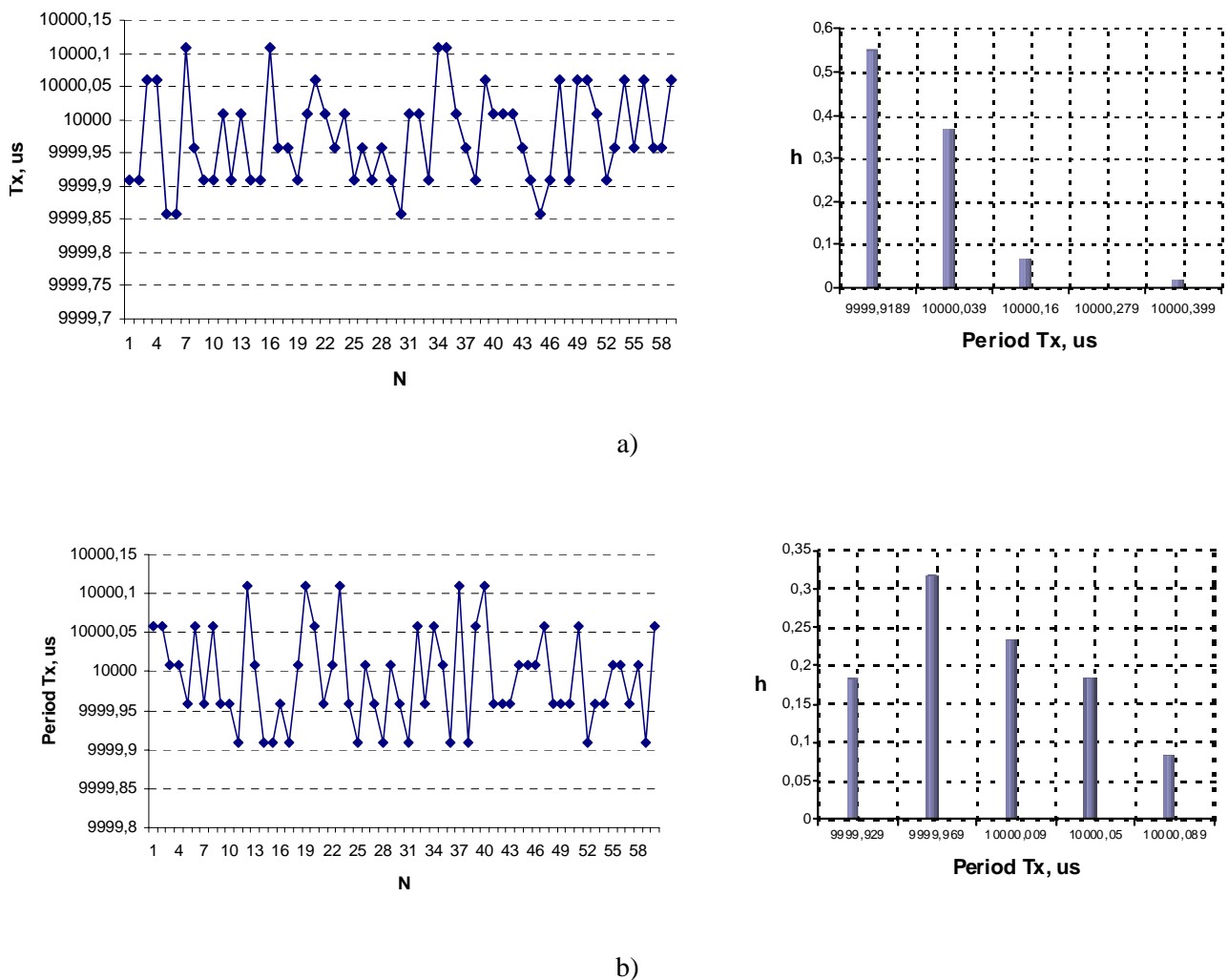


Fig. 5. Experimental results of direct period measurement for a triangular waveform signal and its probability density (a); experimental results and probability density with the use of an external Schmitt trigger (b).

Table 2. Statistical characteristics of the results for period measurements (10 ms) of rectangular waveform signal and slow slew rate signals of different waveforms.

Signal Wave Form Parameter	Rectangular		Triangular		Sine		Exponent Rise		Exponent Fall	
	Directly	With Schmitt trigger	Directly	With Schmitt trigger	Directly	With Schmitt trigger	Directly	With Schmitt trigger	Directly	With Schmitt trigger
Minimal T_x (min), μs	9999.9605	9999.9605	9999.859	9999.90	9999.8605	9999.8605	9999.8582	9999.8582	9999.9587	9999.9587
Maximal T_x (max), μs	10000.0105	10000.0105	10000.4588	10000.1089	10000.0605	10000.0605	10000.1082	10000.0582	10000.0587	10000.0587
Sampling Range, T_x (max) - T_x (min), μs	0.05	0.05	0.5999	0.2	0.2	0.2	0.2499	0.2	0.1	0.1
Median	0	0	0	0	0	0	0	0	0	0
Arithmetic Mean, μs	9999.963	9999.9647	9999.9831	9999.9923	9999.9755	9999.9688	9999.9882	9999.9749	9999.9937	9999.9854
Variance, μs	0.0001	0.0002	0.0088	0.0037	0.0021	0.0032	0.0034	0.0029	0.0009	0.0009
Standard Deviation, μs	0.011	0.0139	0.0936	0.0608	0.0454	0.0569	0.0584	0.0534	0.0295	0.0298
Coefficient of Variation	910206.786	717747.766	106806.024	164427.259	220416.908	175875.618	171370.344	187261.309	338555.832	335849.227
Confidence Interval at probability P=97 %	$T_x \in$ [9999.9599÷ 9999.9661]	$T_x \in$ [9999.9607÷ 9999.9686]	$T_x \in$ [9999.9569÷ 10000.0093]	$T_x \in$ [9999.9752÷ 10000.0093]	$T_x \in$ [9999.9628÷ 9999.9882]	$T_x \in$ [9999.9529÷ 9999.9847]	$T_x \in$ [9999.9719÷ 10000.0046]	$T_x \in$ [9999.9599÷ 9999.9898]	$T_x \in$ [9999.9854÷ 10000.002]	$T_x \in$ [9999.977÷ 9999.9937]
Maximal Relative Error, %	$\leq \pm 0.000031$	$\leq \pm 0.00004$	$\leq \pm 0.000262$	$\leq \pm 0.000171$	$\leq \pm 0.000127$	$\leq \pm 0.000159$	$\leq \pm 0.000164$	$\leq \pm 0.00015$	$\leq \pm 0.000083$	$\leq \pm 0.000084$
Distribution low	-	-	-	Uniform	Gaussian	Gaussian	-	Gaussian	-	-

The χ^2 test for goodness of fit test was applied to investigate the significance of the differences between observed data in the histograms and the theoretical frequency distribution for data from a normal, or uniform, population. For the triangular signal, the period of which was measured with the use of a Schmitt trigger as an input device, for five equidistant classes (Fig. 5b) and a probability $P = 97\%$, according to the χ^2 test, $S < \chi^2_{max}$, where $S = 8.6667$ is the sum of deviations between the dataset and the assumed distribution; $\chi^2_{max} = 10$ is the maximum possible allowable deviation in the χ^2 distribution. Hence, the hypothesis of uniform distribution can be accepted.

The experimental results for sine wave signal period measurements and the probability densities are shown in Fig. 6 (a, b). In this case the use of an external Schmitt trigger does not improve the relative error (Table 2). There is a small error increase (from 0.000127 to 0.000159 %), but in neither cases does the relative error does exceed the programmable relative error of $\delta = 0.0005\%$. For the sine waveform signal, at five equidistant classes (Fig. 6a) and a probability $P = 97\%$, according to the χ^2 -Test, $S < \chi^2_{max}$, where $S = 3.6821$ is the sum of deviations between the dataset and the assumed distribution; $\chi^2_{max} = 7.0$ is the maximum possible deviation in the χ^2 distribution. Hence, the hypothesis of Gaussian (normal) distribution can be accepted. In a case in which a Schmitt trigger is used (Fig. 6b), at five equidistant classes and the same probability $P = 97\%$, according to the χ^2 test, $S < \chi^2_{max}$, where $S = 4.2002$ is the sum of deviations between the dataset and the assumed distribution; $\chi^2_{max} = 7.0$ is the maximum possible argument of the χ^2 distribution. Hence, the hypothesis of Gaussian distribution can be also accepted in this case.

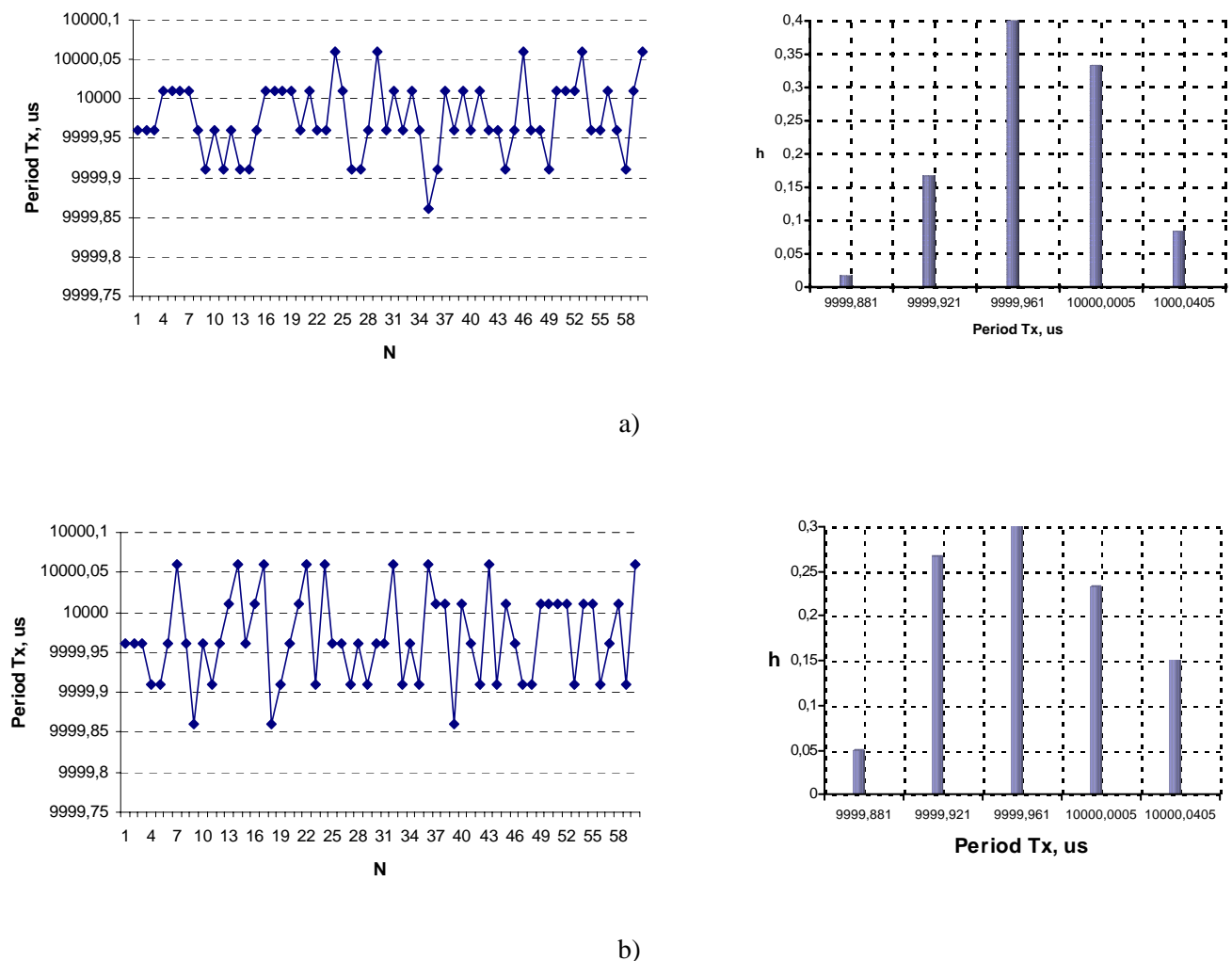


Fig. 6. Experimental results of direct period measurement for sine waveform signal and its probability density (a); experimental results and probability density with the use of an external Schmitt trigger circuit (b).

The experimental results for exponential rise waveform signal period measurements and the probability densities are shown in Fig. 7 (a, b). The similar signal waveform is often used in resistance, capacitance and resistive bridge-to-time interval conversion at the direct sensor-to-microcontroller interfaces based on a charging or discharging capacitor. In case in which an external Schmitt trigger is used (Fig.7b) a small decrease in relative error is observed (Table 2). In this case at five equidistant classes and the probability $P = 97\%$, according to the χ^2 test, $S < \chi^2_{max}$, where $S = 1.9434$ is the sum of deviations between the dataset and the assumed distribution; $\chi^2_{max} = 7.0$ is the maximum possible deviation of the χ^2 distribution. Hence, the hypothesis of Gaussian distribution can be accepted.

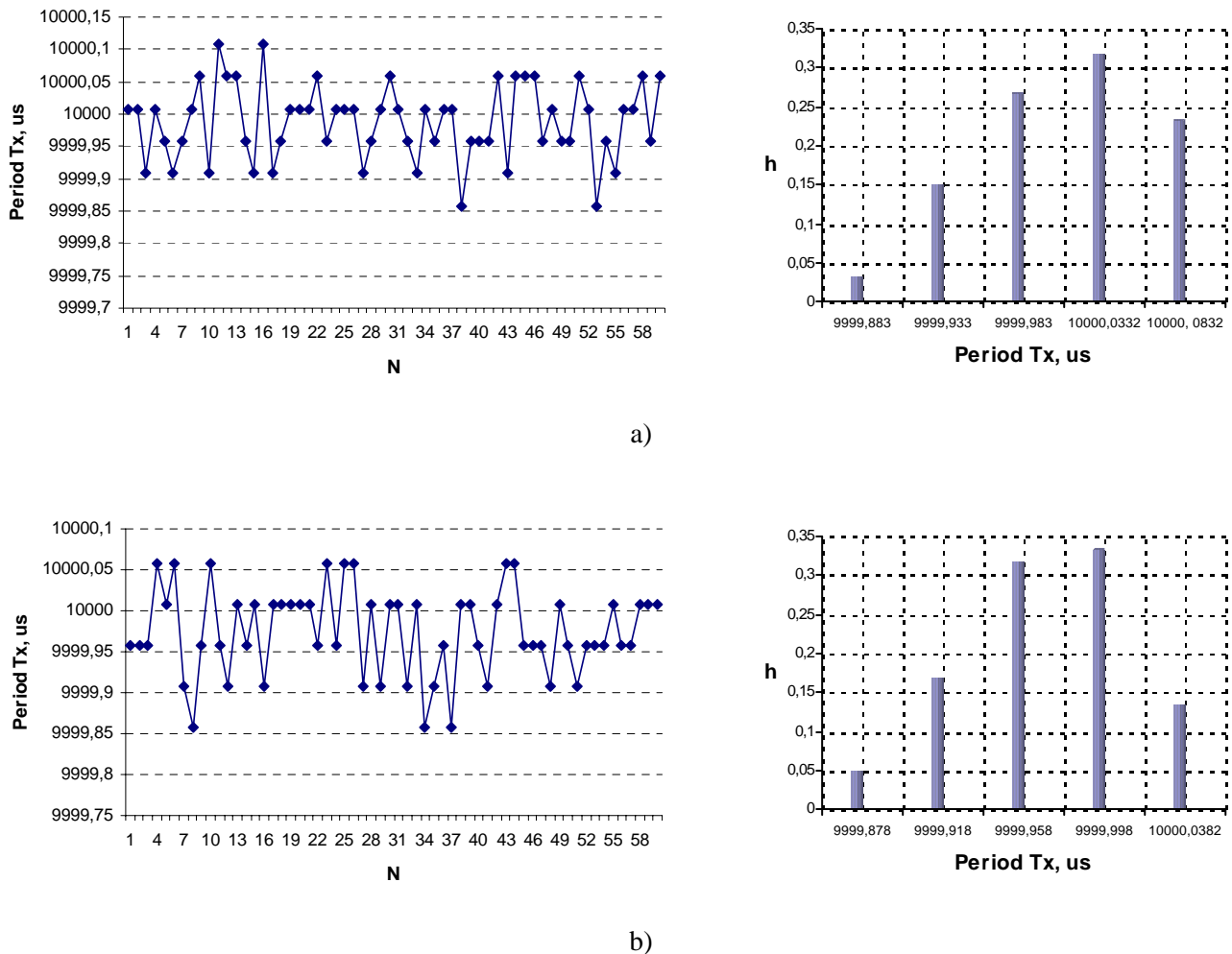


Fig.7. Experimental results of direct period measurement for an exponential rise waveform signal and its probability density (a); experimental results and probability density with the use of an external Schmitt trigger circuit (b).

The experimental results for exponential fall waveform signal period measurements and the probability densities are shown in Fig. 8 (a, b). The use of an external Schmitt trigger as a forming device does not give any relative error improvement (Table 2).

In the case of the rectangular waveform signal, the relative error of period measurements is minimal in comparison with non-rectangular slow slew rate signals and less in 2/8.5 times (Table 2). Nevertheless the use of an external Schmitt trigger decreases the pulse rise time from 24.25 ns to 21.75 ns (Fig. 9), and the use of an external Schmitt-trigger circuit in this case is not recommended (due to the increase in

relative error) because the level of internal noises (thermal noise, interference in the IC power supply, etc.) is greater than the microcontroller's internal noises. Most significant deviations from the arithmetic mean in experimental period measurement results for square wave signals are determined by so-called program-related quantization effects, such as an interrupt response shift in time and interrupt response delay because the interrupt response time depends on the instructions executed by the microcontroller [6]. However, the total relative error does not exceed the programmable one.

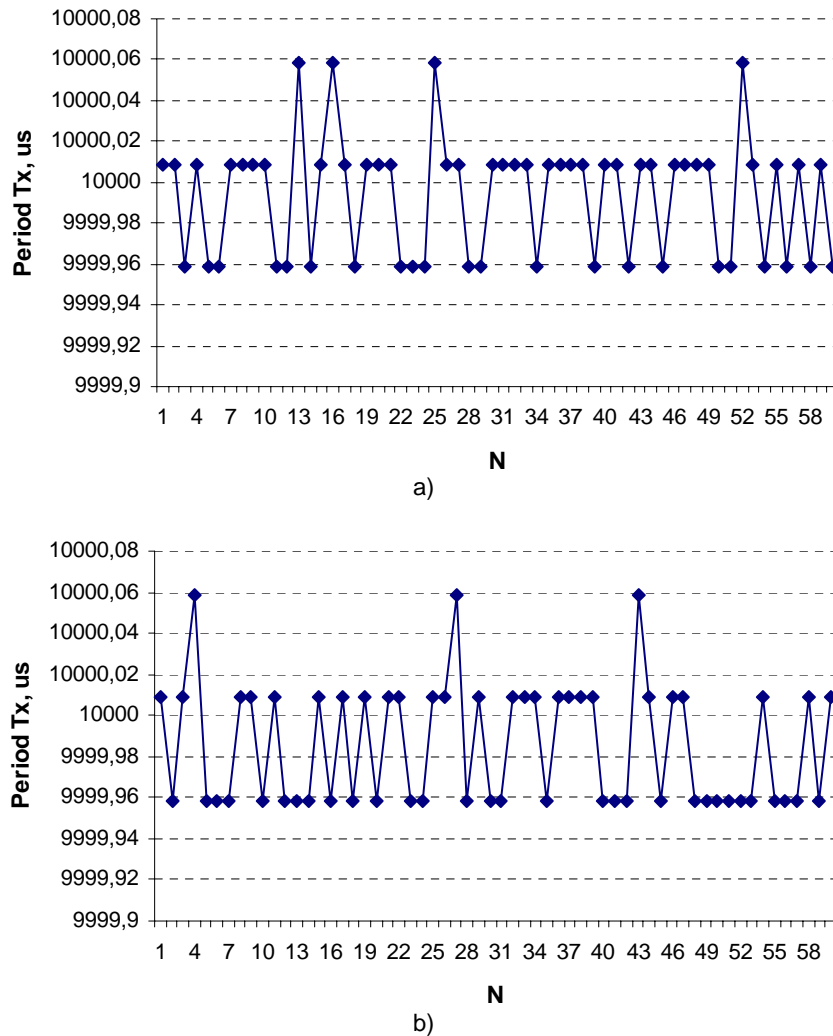


Fig.8. Experimental results of direct period measurement for an exponential fall waveform signal (a); experimental results with the use of an external Schmitt trigger circuit (b).

These experimental results were compared with those obtained in [3, 8-10] for a 100 Hz triangular signal when measuring the period using the indirect counting method. From the counting results of 10 003 μs and 10 006 μs reported in [3, 9, 10] and 10 003 μs and 10 004 μs reported in [8], the maximum quantization errors were $(0.03 \div 0.06) \%$ and $(0.03 \div 0.04) \%$ respectively. When measuring the same frequency and waveform but applying the modified method of dependent counting implemented with the ATmega168-20PI microcontroller, the maximum relative error was below 0.000262 % (Table 2). In the case of a 100 Hz square wave signal, the relative error reported in [8] was $(0.01 \div 0.03) \%$ in comparison with the maximum relative error obtained in described experiments which did not exceed $\pm 0.000031 \%$ (Table 2).

With regard to the conversion speed, for a 0.016 % relative error, neither of the two methods exceeds one period T_x . Of course, increased accuracy in the case of the modified method of the dependent count will

require increasing conversion time, but, in any case, this time will be non-redundant for the proposed modified method. The reference frequency increase of up to $f_0 = 20$ MHz will significantly reduce the conversion time in the proposed modified method of the dependent count performed with the ATmega168-20PI microcontroller. So, for the relative error $\delta = 0.0005\%$ the conversion time will not exceed one period $T_x = 0.01$ s, which corresponds to the 100 Hz input signal.

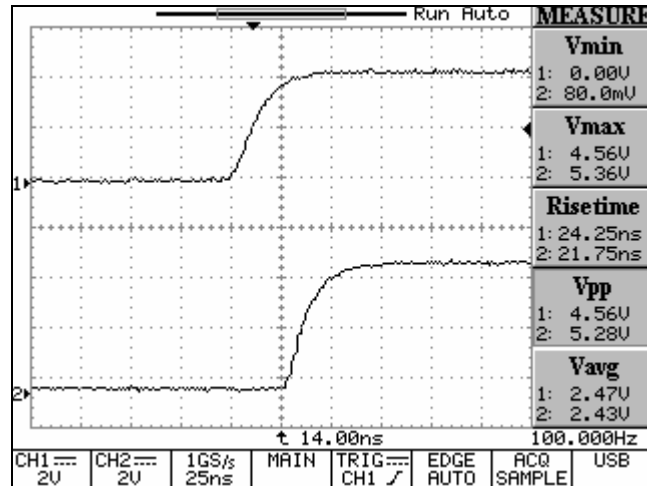


Fig. 9. Rectangular pulse wave front without a Schmitt trigger circuit (1) and with a Schmitt trigger circuit (2).

Even though the relative error can also be reduced slightly by using an external Schmitt trigger, it is not expedient to use this device at a programmable relative error $\geq \delta = 0.0005\%$, because, as is evident from the Table 2, for any investigated signals the relative error without the Schmitt trigger does not exceed the programmable relative error of $\delta = 0.0005\%$. If the modified method of the dependent count described in this article is used, it is also not necessary to use other uncertainty reduction techniques, such as sleep and capture modes for a microcontroller, which are described in [8, 9].

Numerous experiments with the microcontroller-based period measuring systems for rectangular and slow slew rate signals of different waveforms based on the proposed advanced method for frequency (period) and the common ATmega168-20PI microcontroller have also confirmed the high measurement performance of this approach in all frequency ranges possible for this type of microcontroller. Thus, precision frequency (period) measurements with a relative error that does not exceed $\pm 0.0005\%$ programmable error are possible for the frequency range from 0.03 Hz to 7.5 MHz with the ATmega8-16PI microcontroller and 0.05 Hz to 9.1 MHz with the ATmega168-20PI microcontroller. Experimental results of frequency measurements of rectangular waveform pulses at the limits of the measuring range of the ATmega168-20PI microcontroller are shown in Fig.10 (a, b). Absolute and relative errors for measurements of a minimum possible frequency 0.05 Hz are shown in Fig. 11 (a, b) respectively. Thus, the relative error for high 9 MHz frequency does not exceed 0.00043 % and relative error for infra-low 0.05 Hz frequency does not exceed 0.00009 %.

5. Conclusions

The modified method of the dependent count for frequency-time measurements and the indirect counting method for period measurement can be easily implemented by common one-chip microcontrollers. For signals with non-square waveforms, conversion errors due to internal and external

trigger noise predominate, particularly in the low frequency range (slow slew rate). Program-related quantization effects yield errors even for relatively fast input signals.

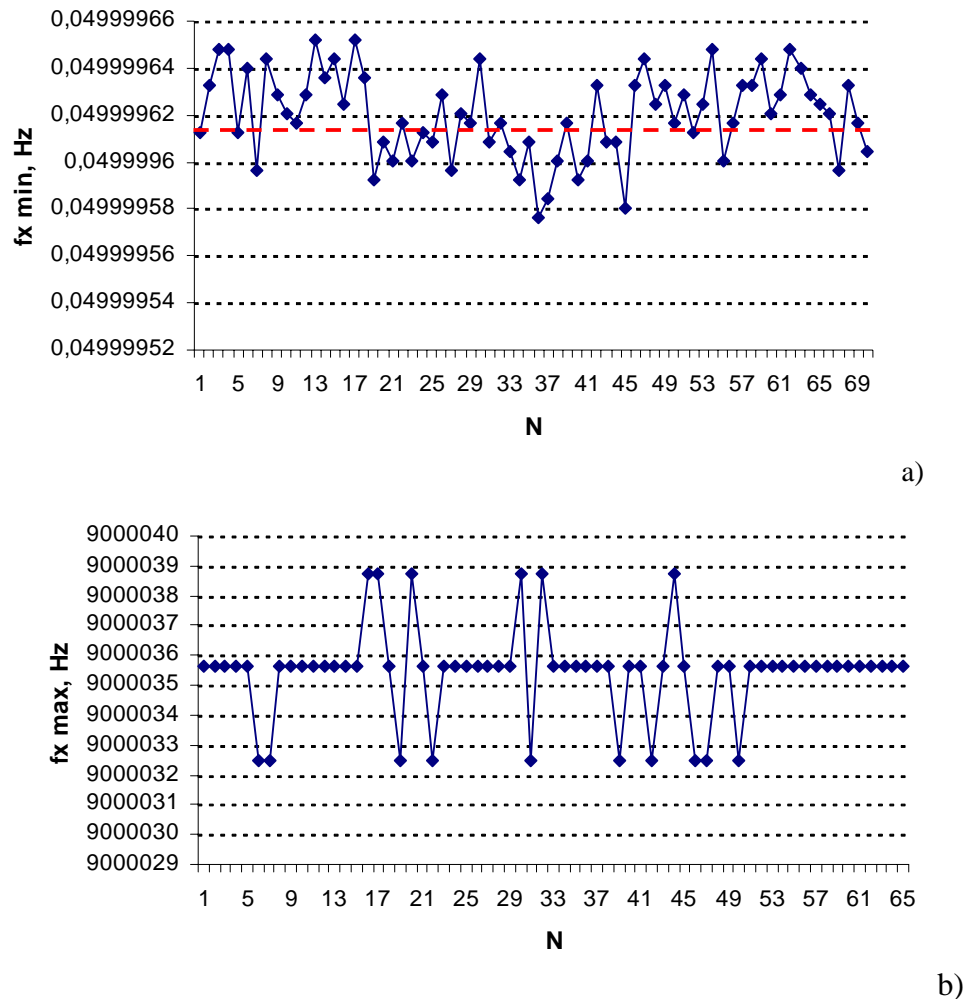
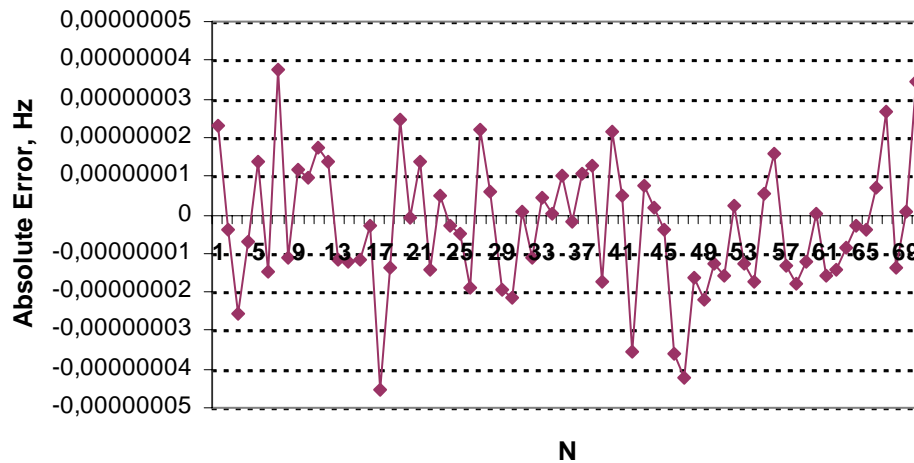


Fig. 10. Experimental results of 0.05 Hz frequency measurements (a); experimental results for 9 MHz frequency measurements (b).

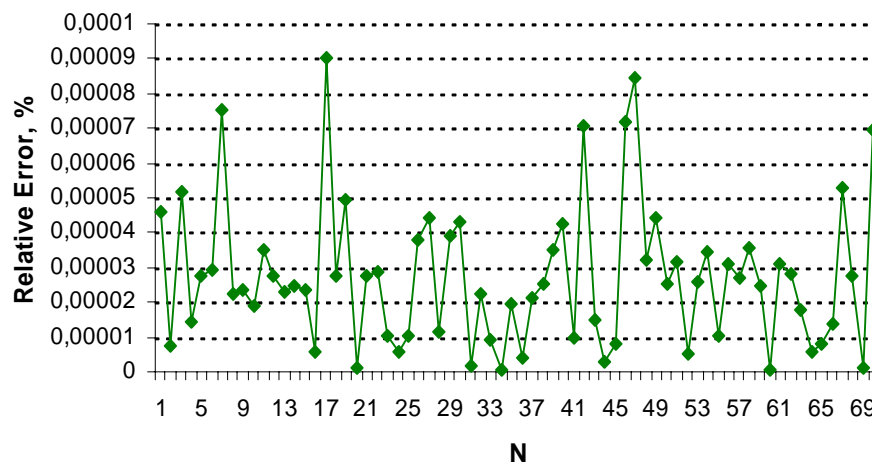
For period measurements of rectangular as well as slow slew rate signals (triangular, sine, exponential rise and exponential fall), the modified method of the dependent count increases the accuracy by 2- to 3-orders as compared to the classical indirect counting method because that method is related to frequency measurement rather than period or single time interval measurements (see time diagrams in Fig. 2). Therefore, components of error, such as trigger uncertainty (Fig. 1) due to internal noise, are either excluded or substantially reduced.

Period measurement is suitable for low frequency measurements due to its non-redundant conversion time. The modified method of the dependent count also has a non-redundant conversion time and for a conversion error $\geq 0.0005\%$ at reference frequency $f_0 = 20$ MHz, its conversion time is the same as for the indirect conversion method: a single period T_x .

For the type of microcontroller used in the experiments described here, the ATmega168-20 PI, precision frequency (period) measurements are possible for the frequency range from 0.03 Hz to 9.1 MHz, with a relative error that does not exceed $\pm 0.0005\%$.



a)



b)

Fig.11. Absolute (a) and relative (b) errors of measurement for 0.05 Hz (0.049999617 Hz) frequency measurements.

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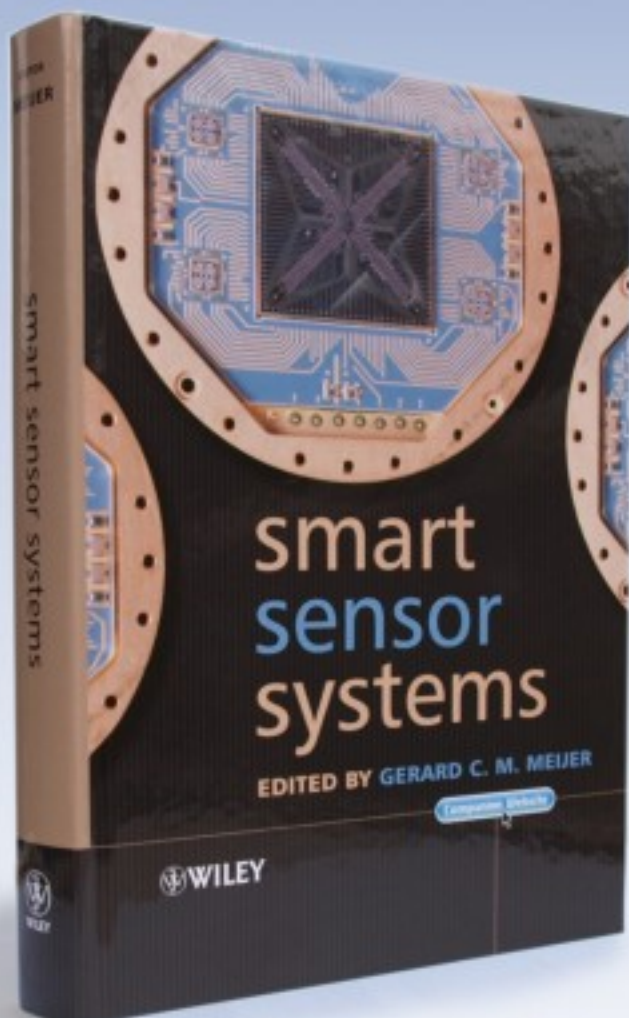
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