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Photogrammetric Resection Approach Using Straight Line Features for Estimation of Cartosat-1 Platform Parameters

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Abstract: The classical calibration or space resection is the fundamental task in photogrammetry. The lack of sufficient knowledge of interior and exterior orientation parameters lead to unreliable results in the photogrammetric process. There are several other available methods using lines, which consider the determination of exterior orientation parameters, with no mention to the simultaneous determination of inner orientation parameters. Normal space resection methods solve the problem using control points, whose coordinates are known both in image and object reference systems. The non-linearity of the model and the problems, in point location in digital images are the main drawbacks of the classical approaches. The line based approach to overcome these problems includes usage of lines in the number of observations that can be provided, which improve significantly the overall system redundancy. This paper addresses mathematical model relating to both image and object reference system for solving the space resection problem which is generally used for upgrading the exterior orientation parameters. In order to solve the dynamic camera calibration parameters, a sequential estimator (Kalman Filtering) is applied; in an iterative process to the image. For dynamic case, e.g. an image sequence of moving objects, a state prediction and a covariance matrix for the next instant is obtained using the available estimates and the system model. Filtered state estimates can be computed from these predicted estimates using the Kalman Filtering approach and basic physical sensor model for each instant of time. The proposed approach is tested with three real data sets and the result suggests that highly accurate space resection parameters can be obtained with or without using the control points and progressive processing time reduction. *Copyright © 2008 IFSA.*

Keywords: Cartosat-1, GCPs, Space resection, Kalman filter, St. line equation of normal to 2D & 3D plane

1. Introduction

Cartosat-1 (IRS-P5) satellite, an Indian stereo mission, was launched in 2005 for catering to photogrammetric and cartographic applications. Launched into polar sun-synchronous circular orbit at an altitude of 618 km, the satellite continues to provide stereo data through its twin Panchromatic (PAN) cameras having high resolution of ~2.5 m and a swath of ~30 km. Both the cameras are tilted with respect to the nadir direction in order to get two views in along the track, one at an angle of +26 deg and the other at -5 deg. The camera looking ahead is called Fore camera and the other one looking near nadir is Aft camera. The primary goal and advantage of Cartosat-1 mission is generation of Digital Elevation Model (DEM) for orthoimage production and 3D terrain visualization on a global basis. Push-broom scanning technique is used in Cartosat-1 for acquiring images like in any other IRS satellites.

The imaging geometry of Cartosat-1 is well modeled by photogrammetric collinearity condition. This method is being used in Cartosat-1 Data Product Generation System (DPGS) s/w for generating high accurate data products as well as in Stereo Strip Triangulation System (SSTS) s/w for generation of country wide Digital Elevation Model (DEM) and Triangulated Control Points (TCPs) over a strip of 500 km. GPS based precise control points are used for this purpose. With the available control points and TCPs, data products team continues to study and carry out various approaches for modeling the imaging geometry of Cartosat-1. Some of the approaches undertaken earlier for modeling exterior platform parameters are using *Kalman Filter* [1, 2], Coplanarity model [3] for improving Cartosat-1 data products accuracy, while the most recent exercises carried in this direction is *Kalman Filter (recursive approach)* approach in space resection problem using straight line features [4], to estimate the Cartosat-1 platform parameters and hence improve the geometric accuracy of data products. This method works with linear features identified in the image or line formation using precise control or image points identified in the image plane.

This paper describes the approach adopted for refining platform parameters of Cartosat-1 using line based resection method with *Kalman Filter*. Details of study and mathematical formulations are described in this report. Also, this report brings out results obtained using Cartosat-1 data sets along with summary of investigations and analysis on the proposed approach.

2. Mathematical Model for Space Resection Using Straight Lines as Features

The mathematical formulation on the approach using straight lines as features to solve photogrammetric space resection is described here. An explicit mathematical relation is established between straight lines in image space and object space. The mathematical model adopted for the solution of the space resection problem using straight lines is based on the equivalence between the vector normal to interpretation plane in the image space and vector normal to the rotated interpretation plane in the object space. The interpretation plane is defined as being the plane, which contains the straight line in the object space (L), the projected straight line in the image space (I), and the perspective center (PC) of the camera.

The vector normal to the interpretation plane in the image space is given by

$$\mathbf{N}^I = - [f \cos\theta \ f \sin\theta \ -\rho], \quad (1)$$

where f is the focal length and θ and ρ are the parameters of the straight line in the image plane, using its normal representation ($x \cos\theta + y \sin\theta - \rho = 0$).

The vector \mathbf{n} , normal to the interpretation plane in the object space, is defined by the vector product (symbol \times) of the direction vector of the straight line (\mathbf{d}), \mathbf{PC} denotes the perspective center coordinates, \mathbf{C} is corresponding object points vector and the vector difference ($\mathbf{PC} - \mathbf{C}$) (see Fig. 1): i.e.,

$$\mathbf{n} = \begin{bmatrix} n_x \\ n_y \\ n_z \end{bmatrix} = \mathbf{d} \times [\mathbf{PC} - \mathbf{C}] = \begin{bmatrix} -n.(Y_c - Y_1) + m.(Z_c - Z_1) \\ n.(X_c - X_1) + l.(Z_c - Z_1) \\ -m.(X_c - X_1) + l.(Y_c - Y_1) \end{bmatrix}, \quad (2)$$

where X_c, Y_c, Z_c are the coordinates of the perspective center of the camera; X_1, Y_1, Z_1 are the three-dimensional coordinates of a known point on the straight line; and l, m, n are the components of the direction vector \mathbf{d} of the straight line; all are defined in the object space reference system.

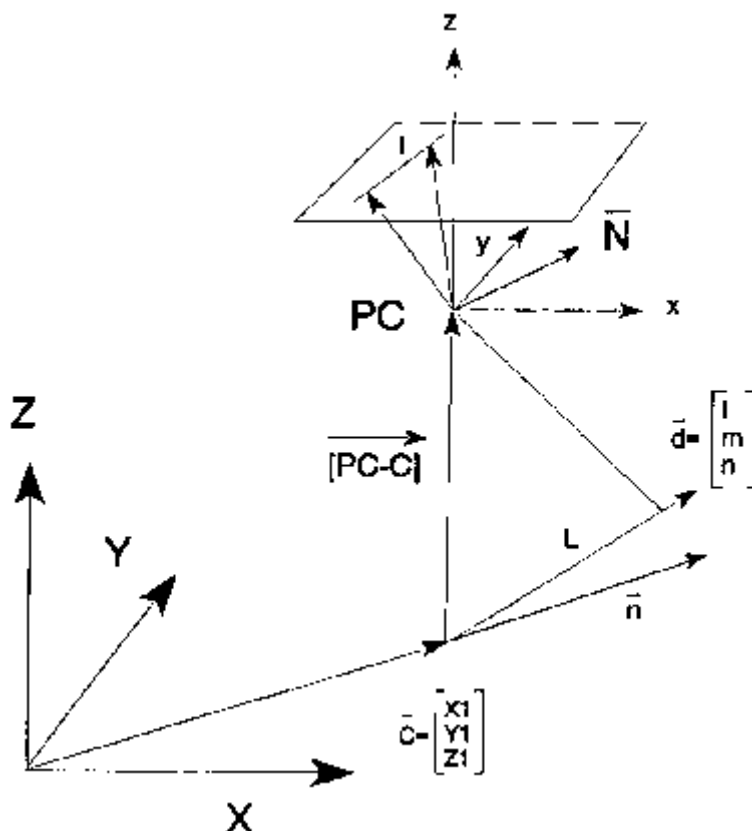


Fig. 1. Vector normal to the interpretation plane in object space and in image space.

Multiplying vector \mathbf{n} by the rotation matrix \mathbf{R} eliminates the angular differences between the object and the image reference systems and results in a vector normal to the interpretation plane in object space that has the same orientation as vector \mathbf{N} , normal to the interpretation plane in the image space, but different in magnitude. Thus,

$$\mathbf{N} = \lambda \mathbf{R} \mathbf{n}, \quad (3)$$

where λ is a scale factor, defined by $\lambda = \|\mathbf{N}\|/\|\mathbf{n}\|$, and \mathbf{R} is the rotation matrix defined by

$$\mathbf{R} = m_1 * m_2 * m_3 \quad (4)$$

m_i 's represents the different transformation matrices from object point to image point conversions (Earth centered inertial to orbit to body to payload system in the way defined for Cartosat-1).

The rotation matrix as in equation (4) can be subdivided into three row vectors: i.e.,

$$\begin{aligned} \mathbf{R}_1 &= [r_{11} \ r_{12} \ r_{13}] \\ \mathbf{R}_2 &= [r_{21} \ r_{22} \ r_{23}] \\ \mathbf{R}_3 &= [r_{31} \ r_{32} \ r_{33}] \end{aligned}$$

where the r_{ij} 's are the elements of the rotation matrix \mathbf{R} , as defined in Equation (4). Using Equation (1) and (2), equation (3) can be rewritten as

$$\begin{bmatrix} f \cdot \cos \theta \\ f \cdot \sin \theta \\ -\rho \end{bmatrix} = -\lambda \begin{bmatrix} r_{11} \cdot n_x + r_{12} \cdot n_y + r_{13} \cdot n_z \\ r_{21} \cdot n_x + r_{22} \cdot n_y + r_{23} \cdot n_z \\ r_{31} \cdot n_x + r_{32} \cdot n_y + r_{33} \cdot n_z \end{bmatrix} \quad (5)$$

Equation (5) can be rewritten as (by eliminating λ)

$$\cot \theta = \frac{r_{11} \cdot n_x + r_{12} \cdot n_y + r_{13} \cdot n_z}{r_{21} \cdot n_x + r_{22} \cdot n_y + r_{23} \cdot n_z} \quad (6)$$

$$\frac{-\rho}{f \cdot \sin \theta} = \frac{r_{31} \cdot n_x + r_{32} \cdot n_y + r_{33} \cdot n_z}{r_{21} \cdot n_x + r_{22} \cdot n_y + r_{23} \cdot n_z}$$

Using the relationships between the elements of the normal vector and the parametric representation of the straight line in the image, equation (6) can be rewritten as

$$\mathbf{a} = -\frac{r_{11} \cdot n_x + r_{12} \cdot n_y + r_{13} \cdot n_z}{r_{21} \cdot n_x + r_{22} \cdot n_y + r_{23} \cdot n_z} \quad (7)$$

$$\mathbf{b} = -f \frac{r_{31} \cdot n_x + r_{32} \cdot n_y + r_{33} \cdot n_z}{r_{21} \cdot n_x + r_{22} \cdot n_y + r_{23} \cdot n_z},$$

where the elements of the parametric equation ($y = ax + b$) are

$$\mathbf{a} = -\cot \theta \text{ and } \mathbf{b} = \rho / \sin \theta$$

$$\tan \theta = \frac{r_{21} \cdot n_x + r_{22} \cdot n_y + r_{23} \cdot n_z}{r_{11} \cdot n_x + r_{12} \cdot n_y + r_{13} \cdot n_z} \quad (8)$$

$$\frac{\rho}{f \cdot \cos \theta} = \frac{r_{31} \cdot n_x + r_{32} \cdot n_y + r_{33} \cdot n_z}{r_{11} \cdot n_x + r_{12} \cdot n_y + r_{13} \cdot n_z}$$

In this case, a new parameters for the straight line must be introduced: i.e.,

$$\mathbf{x} = \mathbf{a}^* \mathbf{y} + \mathbf{b}^*, \quad (9)$$

where

$$\mathbf{a}^* = -\tan \theta \text{ and} \quad (10)$$

$$\mathbf{b}^* = \rho / \cos \theta \quad (11)$$

Using the equations (10) and (11), equation (8) can be rewritten as

$$\mathbf{a}^* = - \frac{r_{21} \cdot n_x + r_{22} \cdot n_y + r_{23} \cdot n_z}{r_{11} \cdot n_x + r_{12} \cdot n_y + r_{13} \cdot n_z} \quad (12)$$

$$\mathbf{b}^* = - f \frac{r_{31} \cdot n_x + r_{32} \cdot n_y + r_{33} \cdot n_z}{r_{11} \cdot n_x + r_{12} \cdot n_y + r_{13} \cdot n_z}.$$

This Equation (12) form the basic mathematical model used for making the partial derivative matrix, which is used as input for *Kalman Filter* recursive approach.

3. Kalman Filter Application to the Resection Problem

For dynamic systems, if the estimate for the motion parameters were available, it would be feasible for the extension of the recursive procedure to the next instant (next image). Using the system model, the estimated motion parameters and the filtered state (camera orientation parameters), the feature position is predicted for the next instant and the new position are computed.

From the earlier study and experiments conducted for Cartosat-1 with various approaches, the bias error is observed large in attitude components than any other error sources. Therefore, this approach is implemented to estimate the biases in roll, pitch and yaw components. Also, the IEKF (Iterated Extended *Kalman Filtering*) is a recursive method used for state estimation, which enables an observation to be processed once it becomes available. This property makes feasible the proposed recursive strategy in which feature identification in the image is improved by better state estimates. The original *Kalman Filter* approach [1] used for estimating attitude components for Cartosat-1 has been modified for the present study.

The application of the IEKF to the space resection model results in the following dimensions for matrices and vectors:

$$\mathbf{X}_{3 \times 1} \quad \mathbf{M}_{2 \times 3} \quad \mathbf{P}_{3 \times 3} \quad \mathbf{K}_{3 \times 2} \quad \mathbf{Z}_{2 \times 1},$$

where

$\mathbf{X}_k = [\boldsymbol{\kappa}, \boldsymbol{\varphi}, \boldsymbol{\omega}]^T$ is taken as a state vector defining the orientation (roll, pitch & yaw) of camera at time t_k ,

$\mathbf{Z}_k^j = [a, b]^T$ are the observations vector for the j^{th} feature in the image at time t_k ,

\mathbf{K} is the Kalman Gain matrix,

\mathbf{M} is the partial derivative matrix and

\mathbf{P} is the state covariance matrix.

Using this notation, Equations (7) and (12) can be rewritten as

$$\mathbf{a} = -\frac{r_{11}.n_x + r_{12}.n_y + r_{13}.n_z}{r_{21}.n_x + r_{22}.n_y + r_{23}.n_z} = -\frac{R_1.n}{R_2.n} \quad (13)$$

$$\mathbf{b} = -f \cdot \frac{r_{31}.n_x + r_{32}.n_y + r_{33}.n_z}{r_{21}.n_x + r_{22}.n_y + r_{23}.n_z} = -f \frac{R_3.n}{R_2.n}$$

$$\mathbf{a}^* = -\frac{r_{21}.n_x + r_{22}.n_y + r_{23}.n_z}{r_{11}.n_x + r_{12}.n_y + r_{13}.n_z} = -\frac{R_2.n}{R_1.n} \quad (14)$$

$$\mathbf{b}^* = -f \frac{r_{31}.n_x + r_{32}.n_y + r_{33}.n_z}{r_{11}.n_x + r_{12}.n_y + r_{13}.n_z} = -f \frac{R_3.n}{R_1.n},$$

where f is the camera focal length, \mathbf{n} is the vector normal to the interpretation plane in the object space, and \mathbf{a} and \mathbf{b} (\mathbf{a}^* and \mathbf{b}^*) are the observations, defined as

$$\mathbf{a} = G_1(x_k) = -\frac{R_1.n}{R_2.n} = -\frac{v}{u} \text{ (say)} \quad (15)$$

$$\mathbf{b} = G_2(x_k) = -f \frac{R_3.n}{R_2.n} = -f \frac{w}{u} \text{ (say)}$$

$$\mathbf{a}^* = F_1(x_k) = -\frac{R_2.n}{R_1.n} = -\frac{u}{v} \quad (16)$$

$$\mathbf{b}^* = F_2(x_k) = -f \frac{R_3.n}{R_1.n} = -f \frac{R_3.n}{R_1.n} = -f \frac{w}{v}$$

For the measurement model as stated in equation (15), \mathbf{M} matrix can be obtained by the partial derivatives of the measurement model with respect to the elements of the state vector as

$$\mathbf{M} = \begin{bmatrix} \frac{\partial F_1}{\partial \kappa} & \frac{\partial F_1}{\partial \phi} & \frac{\partial F_1}{\partial \omega} \\ \frac{\partial F_2}{\partial \kappa} & \frac{\partial F_2}{\partial \phi} & \frac{\partial F_2}{\partial \omega} \end{bmatrix},$$

where

$$\frac{\partial F_1}{\partial x_i} = -\frac{R_2'.n.R_1.n - R_2.n.R_1'.n}{(R_1.n)^2}$$

$$\frac{\partial F_2}{\partial x_i} = -f \frac{R_3'.n.R_1.n - R_3.n.R_1'.n}{(R_1.n)^2} \quad i=1,2, \dots,6$$

and x_i is an element of the state vector, ' (dash) denotes differentiation w.r.t state vectors.

The derivative of the rotation matrix with respect to state elements is

$$\begin{aligned}\frac{\partial R_1}{\partial \kappa} &= R_2, \quad \frac{\partial R_1}{\partial \phi} = -R_3 c\kappa, \quad \frac{\partial R_1}{\partial \omega} = [0 \quad -r_{13} \quad r_{12}], \\ \frac{\partial R_2}{\partial \kappa} &= -R_1, \quad \frac{\partial R_2}{\partial \phi} = R_3 s\kappa, \quad \frac{\partial R_2}{\partial \omega} = [0 \quad -r_{23} \quad r_{22}], \\ \frac{\partial R_3}{\partial \kappa} &= 0, \quad \frac{\partial R_3}{\partial \phi} = [c\phi \quad s\omega.s\phi - c\omega.s\phi], \quad \frac{\partial R_3}{\partial \omega} = [0 \quad -r_{33} \quad -r_{32}].\end{aligned}$$

where $c_i = \cos i$ and $s_i = \sin i$ (i represents angle).

The partial derivative of the measurement model (Equation (15) with respect to the rotations are

$$\begin{aligned}\frac{\partial F_1}{\partial \kappa} &= 1 + \frac{u^2}{v^2}, \quad \frac{\partial F_2}{\partial \kappa} = f \cdot \frac{w.u}{v^2}, \quad \frac{\partial F_1}{\partial \phi} = -\frac{s\kappa.w.v + c\kappa.w.u}{v^2}, \\ \frac{\partial F_2}{\partial \phi} &= -f \frac{(c\phi.n_x + s\omega.s\phi.n_y - c\omega.s\phi.n_z).v + c\kappa^2.w}{v^2}, \\ \frac{\partial F_1}{\partial \omega} &= -\frac{(r_{23}.n_y - r_{22}.n_z).v - u.(-r_{13}.n_y + r_{12}.n_z)}{v^2}, \\ \frac{\partial F_2}{\partial \omega} &= -f \frac{(r_{33}.n_y + r_{32}.n_z).v - w.(-r_{13}.n_y + r_{12}.n_z)}{v^2}.\end{aligned}$$

The partial derivative for the measurement model are obtained and given as input to the sequential estimator as an initial estimate. The complete implementation approach is described in the next section.

4. Methodology

While implementing the above described model for Cartosat-1, the following points are considered viz.

1. The laboratory calibrated interior orientation parameters of both cameras are precisely known and they are used in this approach.
2. Ground Control Points(GCPs)' precise positions are known in the image(strip of 500 km) along with their GPS ground position. The object model is known by treating 2 GCPs as the end points of straight line corresponding to the two end points in the image plane. Also, the approach has been attempted with estimated ground positions of the two image points by treating them as straight line (joining the end points of two consecutive points) and this is to prove that only the image points are sufficient for estimating the platform parameters.
3. For initial approximation, a priori estimates of orientation parameters are taken from Cartosat-1 ancillary data.

4. At the initial time t_0 , the priori estimate for state vector x_0 and its covariance matrix p_0 are assigned to variables x_{k-1} and p_{k-1} respectively.
5. Using the predicted state vector estimate x_k a perspective transformation is applied to the endpoints of all straight lines in the object model.

Let $x_k = [\kappa, \varphi, \omega]$ be the state vector defining the camera orientation at time t_k and p_k its covariance matrix, and let $z_k^j = [a^*, b^*]^T$ be the observation vector for the j^{th} feature in the image.

The filtered state parameters and their covariance matrix obtained using the j^{th} observation are used as the predicted values for the $(j+1)^{\text{th}}$ observation to update the perspective transformation from object to image space. After each iteration, the filtered state parameters obtained are better than the previous ones; hence, the displacement between the acquired image feature and the projected one is progressively reduced, resulting in a reduction of RMS error corresponding to each iteration. This procedure is repeated until all available lines have been processed. In our study, we have used only 4 points i.e. two straight lines, which is the minimum requirement by the model.

After platform parameters are updated by the *Kalman Filter* based resection model using lines as features, ground to image (G2I) mapping is used to evaluate the performance of the model by considering all other GCPs as check points.

5. Results and Discussions

Space resection approach with the help of sequential estimator (*Kalman Filter*) using straight line features for improving Cartosat-1 platform parameters is discussed here. The study includes various experiments conducted with different Cartosat-1 stereo data sets and analysis of the results achieved. The exercises were carried out for 3 data sets of Cartosat-1 with the help of a few control points from stereo pair (Table 1). Though control points are necessary for absolute calibration of platform parameters, this method was tried without using control points also (Table 2). Modeling the attitude parameters were carried out with and without control points while performance of this method was assessed using different set of control points as check points. Results were evaluated at check points at both pre and post model level. Statistical criteria viz. both RMS error and standard deviation (Std. Dev) were used for assessing accuracy measures. Results of pre adjustment (system level using Cartosat-1 onboard measured attitudes) are compared with post resection level (using improved attitudes) for both cases of with and without GCPs for each data set.

The following conclusions are derived from the present experiments conducted for Cartosat-1.

1. As can be seen from Table 1, post resection results show good improvement in terms of RMS error for both along and across directions. This confirms that biases present in attitude are better estimated by the proposed approach. This is seen for all the three data sets for both Fore and Aft cameras.
2. The overall behavior of the platform parameters (roll, pitch and yaw) are shown for one particular case (date of pass: 28th May 2005) in Fig. 2 (Fore) and Fig. 3 (Aft).
3. Further, it is clear from Table 1 that standard deviation at both pre & post level are nearly same in pixel direction whereas it is not so for scan direction. There is slight deterioration in scan direction. This could be due to the fact that the model does not use higher order attitude variation, as it estimates biases only using two line features. More number of line features may be necessary and this is to be tested.
4. It is observed that Aft camera post results are better than Fore camera results for all cases. However, it can be concluded that the overall accuracy of the model is well within 10 pixels for both

directions, which is better than the system level accuracy. Additional testing, experiments and investigations are required for improving further.

5. From Table 2, it can be seen that without using the actual control points it is possible to refine the biases for attitude components. More testing is required in this direction.
6. It is to be noted that the points considered for modeling are lying between 0.4 seconds to maximum 5.0 seconds while check points for accuracy evaluation are taken from extrapolated region, in the range of 1.0 to 10 seconds

The sequence of steps followed for this recursive approach to the solution of the space resection problem is described in the flow chart (Fig. 4).

Table 1. Pre- and Post- resection results.

DOP	Cameras	Rms scan (in pixel)		Rms pix (in pixel)		Std. scan (in pixel)		Std. pix (in pixel)	
		Pre	Post	Pre	Post	Pre	Post	Pre	Post
28 th May	Fore	47.49	7.95	3.47	5.48	2.47	7.94	3.12	2.87
	Aft	30.48	3.27	9.72	3.19	2.22	2.18	3.53	3.11
8 th June	Fore	29.86	6.67	5.84	2.27	3.05	6.61	2.30	2.27
	Aft	12.69	2.47	3.21	1.81	2.13	2.09	1.86	1.79
4 th Nov.	Fore	29.13	9.35	10.39	1.32	1.48	3.06	1.44	1.32
	Aft	17.20	3.46	26.77	1.002	1.06	2.84	1.10	0.96

Table 2. Results of resection without using control points.

DOP	Cameras	Rms scan (in pixel)		Rms pix (in pixel)		Std. scan (in pixel)		Std. pix (in pixel)	
		Pre	Post	Pre	Post	Pre	Post	Pre	Post
28 th May	Fore	47.49	7.92	3.47	2.50	2.47	7.53	3.12	2.26
	Aft	30.48	2.42	9.72	3.35	2.22	2.07	3.53	1.79
8 th June	Fore	29.86	13.02	5.84	3.06	3.05	8.03	2.30	2.85
	Aft	12.69	6.64	3.21	3.11	2.13	2.18	1.86	3.11

6. Conclusions

The sequential iterative filter technique has been tested for estimation of Cartosat-1 platform parameters, which uses straight lines for space resection purpose. Three data sets have been used and promising results are obtained with and without using control points. More exercises and analysis are required to understand this method for various realistic imaging conditions. The preliminary results are only presented in this report Further scope exists to extend this method for longer duration, handling higher order variations in attitude, modeling state vector (position of perspective center) and incorporation of edge detection technique for line feature identification.

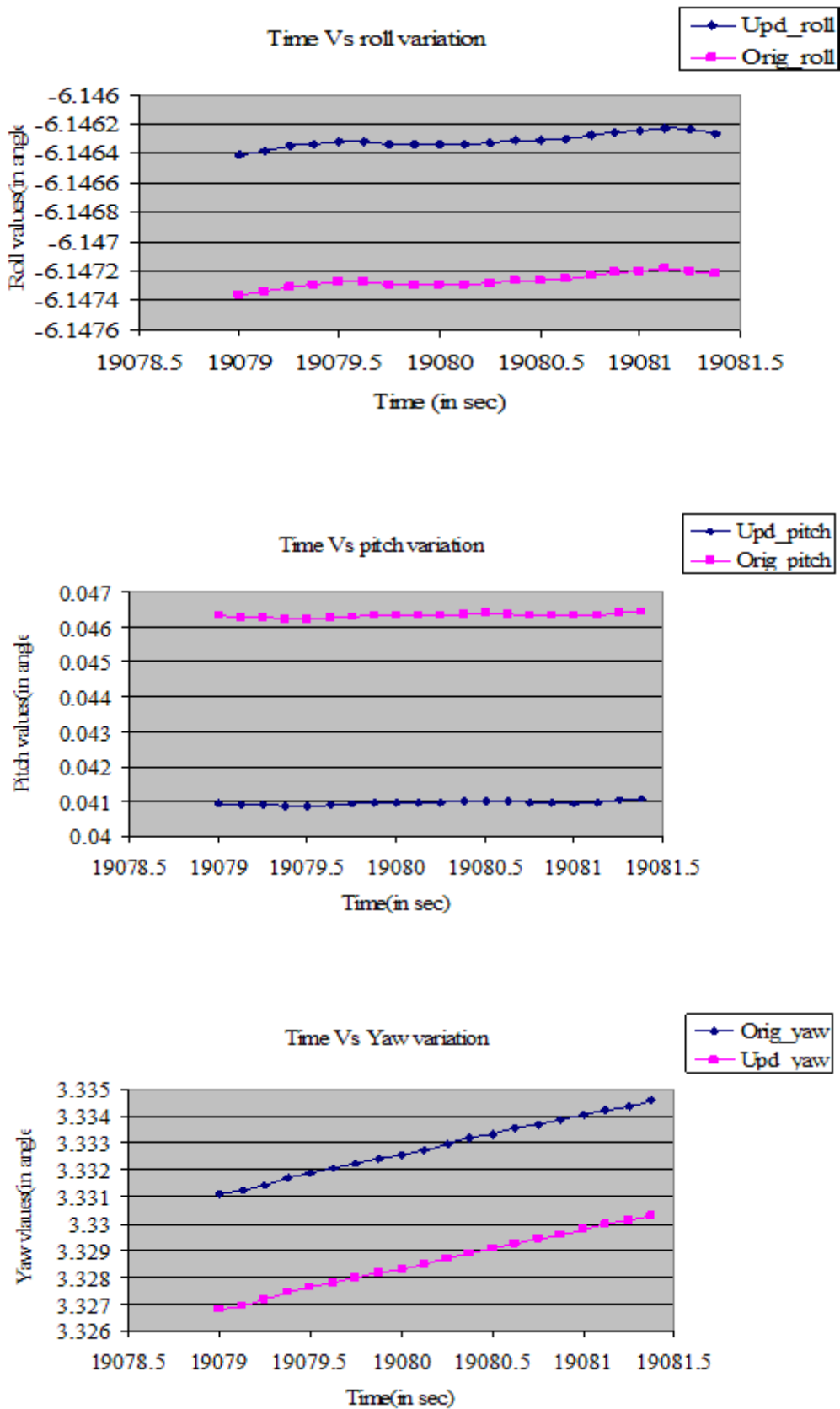


Fig. 2. Plots of Fore Camera Roll, Pitch & Yaw.

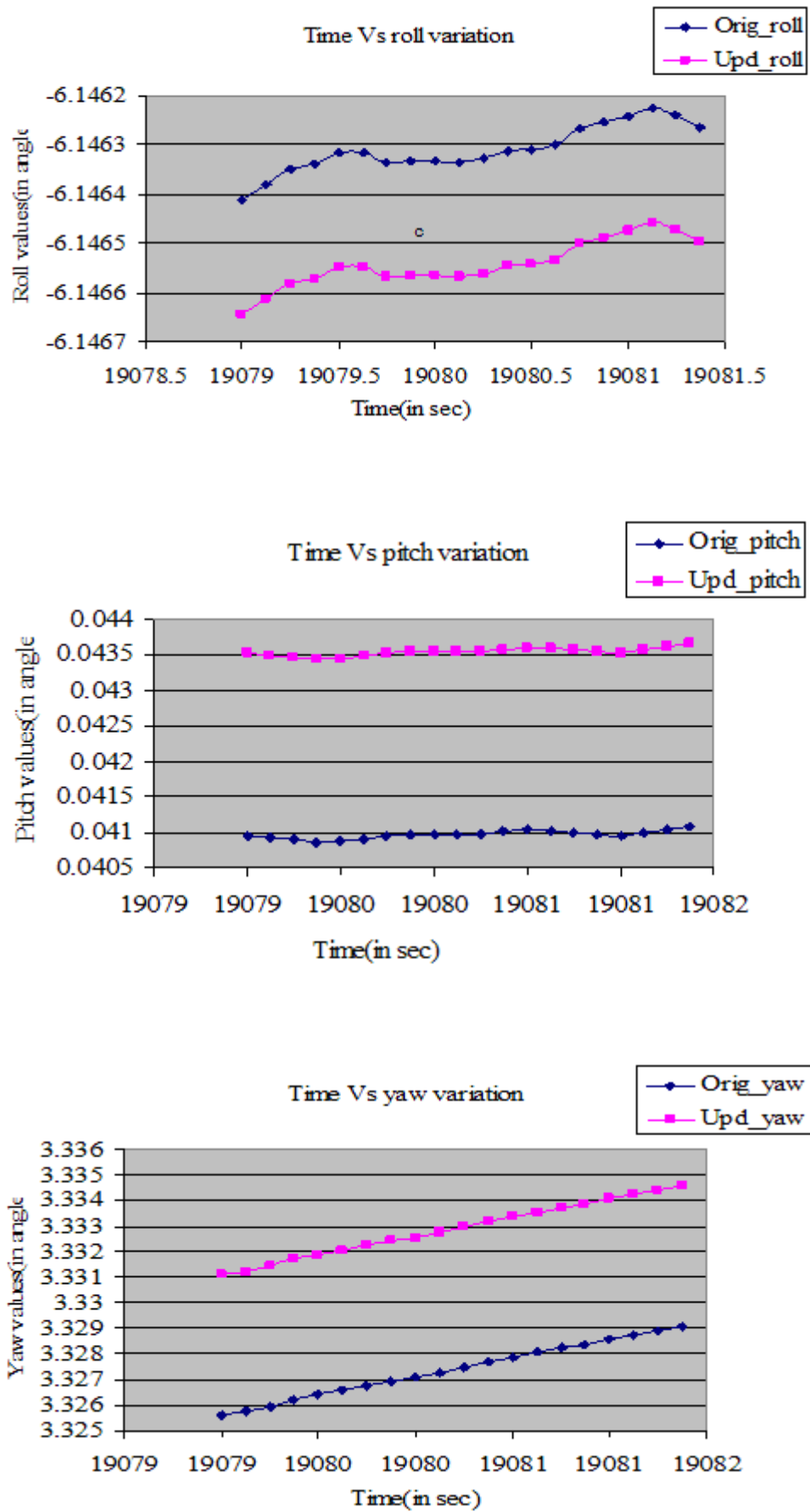


Fig. 3. Plots of Aft Camera Roll, Pitch & Yaw.

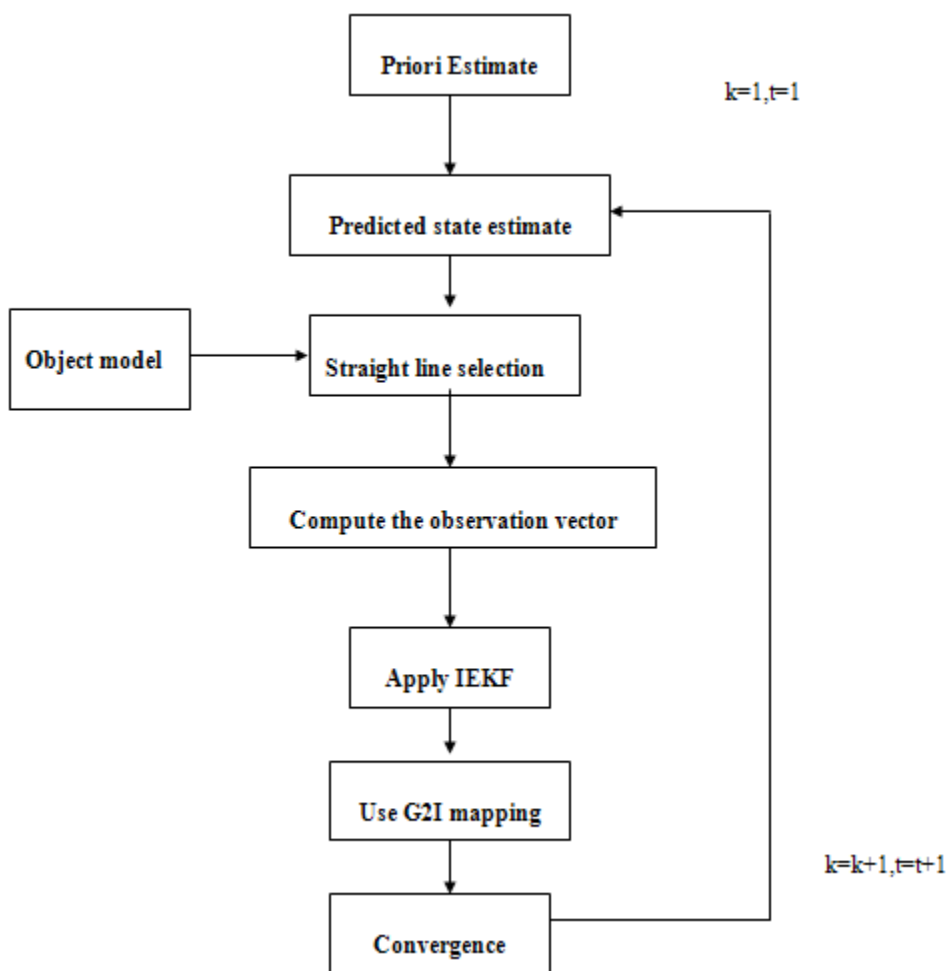


Fig. 4. Kalman Filter recursive procedure using lines for space resection.

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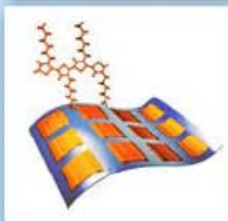
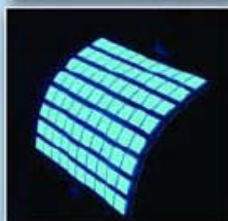
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