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The background of the cover features a green-tinted image of several microchips mounted on a circuit board. The chips are arranged in a perspective view, with some in the foreground and others receding into the background. Each chip has the letters 'USTI' printed on its top surface. Numerous yellow and green lines, representing circuit traces, radiate from the chips, creating a sense of connectivity and data flow. The overall aesthetic is high-tech and futuristic.

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Design and Implementation of Output Feedback Control for Piezo Actuated Structure Using Embedded System

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Abstract: This paper presents the design of periodic output feedback control using state feedback gain to control the vibration of piezo actuated cantilever beam. The effectiveness of the controller is evaluated through simulation and experimentally by exciting the structure at resonance. Real time implementation of the controller is done using microcontroller. The closed loop eigen values of the system with periodic output feedback and state feedback are identical. *Copyright © 2008 IFSA.*

Keywords: State feedback, Periodic output feedback, Piezoelectric, Smart structure

1. Introduction

Vibrations can be found virtually everywhere, in vehicles, buildings, or machines, flexible structures. Most vibrations are undesirable because they cause unpleasant noises, unwanted stress in structures, and failure of systems. Within the last two decades, much attention has been focused on active control of structures to suppress their structural vibrations. The use of piezoelectric actuators and sensors has shown promising applications in active vibration control of flexible structures [1-2]. These materials in particular piezoceramics (PZT) are attractive for distributed actuators and sensors because they combine small size, low energy consumption, fast response, high efficiency, excellent sensing and significant actuation capabilities and exhibit favorable bonding characteristics. These advantages have encouraged researchers to establish models for flexible structures (Plate, shell, beam) that incorporate piezoelectric actuators/sensors [3-4]. Distributed piezoelectric materials experimentally have proven to be practical in sensing and controlling the vibrations of flexible structures [5-6]. The state feedback controller needs either the availability of the state vector or an estimator but output feedback requires only measurement of the system output. The periodic output feedback control has been implemented

for vibration suppression of smart structure cantilever beam [7-8]. The periodic output feedback gain has computed from state feedback gain and closed loop eigen values are same [9]. In this paper, a periodic output feedback controller is designed from the state feedback controller for vibration suppression of piezo actuated cantilever beam and the effectiveness of the controller is evaluated through simulation and experimentally by exciting the structure at resonance.

2. Experimental Set-up and Its Model

A flexible aluminum beam with clamped end as shown in Fig. 1. is considered in this paper. Two piezo ceramic patches are bonded at a distance of 10 mm from the fixed end of the beam. The patch bonded on the bottom surface acts as a sensor and the one on the top surface acts as an actuator. To apply an excitation input to the structure another piezo ceramic patch is bonded on the top surface at a distance of 387.8 mm from the fixed end. The dimensions and properties of the beam and piezo ceramic patches are given in Table 1.

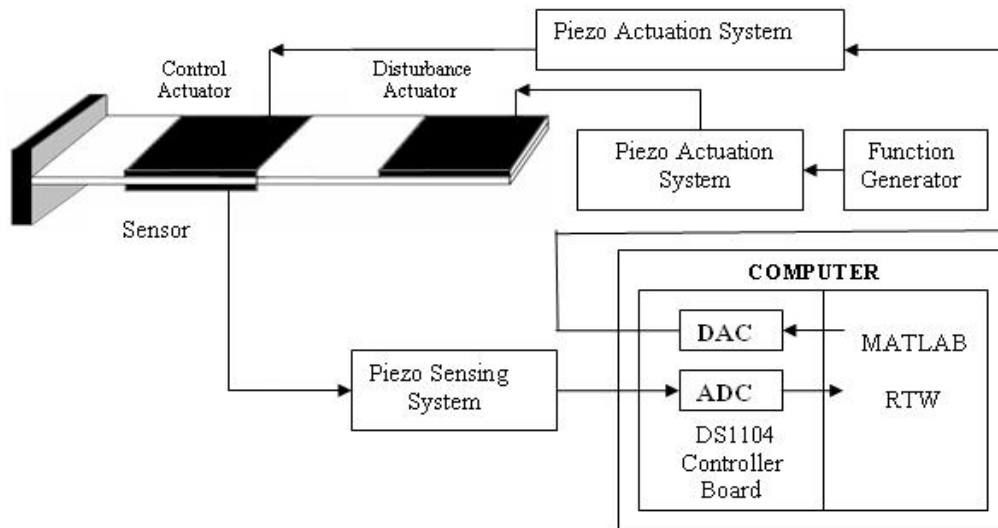


Fig. 1. Schematic diagram of experimental set up.

Table 1. Properties and dimensions of the Aluminium beam and piezoceramic Sensor/Actuator.

Parameter	Aluminium beam	Piezoceramic Sensor/actuator
Length (m)	0.3	0.0765
Width (m)	0.0127	0.0127
Thickness (m)	0.0023	0.005
Young's modulus (Gpa)	71	47.62
Density (kg/m ³)	2700	7500
First natural frequency (Hz)	31.7	----
Piezoelectric strain constant (m V ⁻¹)	----	-247x10 ⁻¹²
Piezoelectric stress constant (V m N ⁻¹)	----	-9x10 ⁻³

The sensor output is given to the piezo sensing system which consists of charge to voltage converting amplifier. The conditioned piezo sensor signal is given as analog input to dSPACE1104 controller board. The model of a cantilever beam in Fig. 1 is obtained using recursive least square (RLS) method

based on ARX model [7]. The excitation signal, input signal and sensor output are given to MATLAB/Simulink through ADC port of dSPACE 1104 system. The RLS algorithm is implemented by writing a C-file S-function used in MATLAB/Simulink. The state space model derived from the identified second order ARX model parameters is

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{b}u + \mathbf{e}r; \quad y = \mathbf{c}^T \mathbf{x}, \quad (1)$$

where

$$\mathbf{A} = \begin{bmatrix} -83.0583 & 218.2890 \\ -204.9014 & 76.7292 \end{bmatrix}, \quad \mathbf{b} = \begin{bmatrix} -1.4349 \\ -1.708 \end{bmatrix}, \quad \mathbf{e} = \begin{bmatrix} -0.2359 \\ -0.0477 \end{bmatrix}, \quad \mathbf{c}^T = [1 \quad 0].$$

3. Review of Periodic Output Feedback Controller

Consider a linear continuous-time invariant state space model:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{b}u; \quad y = \mathbf{c}^T \mathbf{x}, \quad (2)$$

where $\mathbf{x} \in \mathfrak{R}^n$, $u \in \mathfrak{R}^m$, $y \in \mathfrak{R}^p$ and \mathbf{A} , \mathbf{b} and \mathbf{c}^T are constant matrices. It is assumed that $(\mathbf{A}, \mathbf{b}, \mathbf{c}^T)$ is controllable and observable. Assume that output measurements are available from the system in equation (1) at time instants $t = k\tau$, where $k=0,1,2,\dots$. Now design an output injection gain matrix \mathbf{G} , such that the eigen values of $(\Phi_\tau + \mathbf{G}\mathbf{c}^T)$ are inside the unit circle. For the system $(\Phi_\tau, \Gamma_\tau, \mathbf{c}^T)$ the control signal is generated according to

$$\begin{aligned} u(t) &= \mathbf{K}_l y(k\tau), \\ k\tau + l\Delta \leq t < k\tau + (l+1)\Delta, \quad \mathbf{K}_{l+N} &= \mathbf{K}_l \end{aligned} \quad (3)$$

for $l = 0, 1, \dots, N-1$, where a sampling interval τ is divided into N subintervals $\Delta = \frac{\tau}{N}$ and N is equal to or greater than the controllability index of (Φ_τ, Γ_τ) . Note that the sequence of gain matrices $\{\mathbf{K}_0, \mathbf{K}_1, \mathbf{K}_2, \dots, \mathbf{K}_{N-1}\}$, when substituted into equation (3), generates a time-varying, piecewise constant output feedback gain $\mathbf{K}(t)$ for $0 \leq t \leq \tau$. To see the relationship between the gain sequence $\{\mathbf{K}_l\}$ and closed loop behavior collect the gain matrices \mathbf{K}_l into one matrix

$$\mathbf{K} = \begin{bmatrix} \mathbf{K}_0 & \mathbf{K}_1 & \cdots & \mathbf{K}_{N-1} \end{bmatrix}^T$$

By applying a control input $u(t)$ as calculated in equation (3), a state space representation for the closed loop system sampled at the rate of $\frac{1}{\tau}$ is

$$\mathbf{x}(k+1) = \Phi^N \mathbf{x}(k) + \Gamma \mathbf{K} \mathbf{c}^T \mathbf{x}(k), \quad (4)$$

where

$$\Gamma = \begin{bmatrix} \Phi^{N-1} \Gamma & \Phi^{N-2} \Gamma & \Phi^{N-3} \Gamma & \dots & \Gamma \end{bmatrix}$$

If (Φ, Γ) system is controllable and $(\Phi_\tau, \mathbf{c}^T)$ observable, one can first choose an output injection gain \mathbf{G} to place the eigen values of $(\Phi_\tau + \mathbf{G} \mathbf{c}^T)$ in the desired locations and then compute the gain sequence $\{\mathbf{K}_1\}$ such that $\Gamma \mathbf{K} = \mathbf{G}$ is satisfied.

Let $(\Phi_\tau, \Gamma_\tau, \mathbf{c}^T)$ be the discrete time system obtained with by sampling the system in equation (1) at a rate $1/\tau$. Let the characteristics polynomial of Φ_τ be represented as

$$p(\Phi_\tau) = S^n + \sum_{i=0}^{n-1} a_i S^i \quad (5)$$

Let the controllable canonical form of the system (1) be $(\Phi_{\tau,c}, \Gamma_{\tau,c}, C_c, Z_c)$. If the state feedback gain $F_c = [f_{c,0} \ f_{c,0} \ \dots \ f_{c,n-1}]$ is designed for this system such that the eigen spectrum of the closed loop system $(\Phi_{\tau,c} + \Gamma_{\tau,c} F_c)$ is $\Lambda = \{\lambda_1, \dots, \lambda_n\}$ then it can be easily shown that

$$p(\Phi_{\tau,c} + \Gamma_{\tau,c} F_c) = S^n + \sum_{i=0}^{n-1} (a_i + f_{c,i}) S^i \quad (6)$$

Similarly, the observable canonical representation of system (1) is $(\Phi_{\tau,o}, \Gamma_{\tau,o}, C_o, Z_o)$. The output injection gain $G_o = [g_{o,0}, g_{o,0}, \dots, g_{o,n}]^T$ is computed $(\Phi_{\tau,o} + G_o C_o)$ has the same eigenspectrum Λ as of the state closed loop controllable canonical form with state feedback gain F_c then

$$p(\Phi_{\tau,o} + G_o C_o) = p(\Phi_{\tau,c} + \Gamma_{\tau,c} F_c) \quad (7)$$

$$S^n + \sum_{i=0}^{n-1} (a_i + g_{o,i}) S^i = S^n + \sum_{i=0}^{n-1} (a_i + f_{c,i}) S^i$$

Comparing the coefficients of $S^i, i = 0, \dots, n-1$, it can be seen that $g_{o,i} = f_{c,i}, i=0, \dots, n-1$,

$$G_o = F_c^T \quad (8)$$

The state feedback gain and output injection gain that have the same effect on the original system $(\Phi_\tau, \Gamma_\tau, c^T, x)$ as F_c and G_o have on its controllable and observable canonical forms respectively, can be computed as

$$\begin{aligned} F &= F_c T_c \\ G &= T_o^{-1} G_o \end{aligned} \quad (9)$$

Now using, the relation between F and G may be derived as

$$G = T_o^{-1} (F T_c^{-1})^T \quad (10)$$

The periodic output feedback gain that would result in the same closed loop poles as a given by state feedback is computed from this,

$$\mathbf{K} = \Gamma^{-1} T_o^{-1} (F T_c^{-1})^T \quad (11)$$

This periodic output feedback gain \mathbf{K} would result in the eigen values of the closed loop system $(\Phi_\tau + \Gamma \mathbf{K} c^T)$ to be the same as those obtained from state feedback F , i.e., eigen vales of the closed loop system $(\Phi_\tau + \Gamma_\tau F)$.

4. Controller Design

The periodic output feedback controller is designed to reduce the amplitude of vibration of the cantilever beam at resonance. A stabilizing output injection gain is designed as explained in Section 3 for the system $(\Phi_\tau, \Gamma_\tau, c^T)$, such that the eigen values of $(\Phi_\tau + Gc^T)$ lie inside the unit circle.

Where

$$\tau = 0.01 \text{ sec and } \Delta = 0.0025 \text{ sec, } N = 4$$

$$\Phi_\tau = \begin{bmatrix} -0.7320 & 1.0000 \\ -0.9387 & -0.0000 \end{bmatrix} \quad \Gamma_{\tau,b} = \begin{bmatrix} -0.0158 \\ -0.0025 \end{bmatrix}$$

$$\Gamma_{\tau,e} = \begin{bmatrix} -0.0008 \\ 0.0013 \end{bmatrix} \quad c^T = [1 \quad 0]$$

$$F = [0.4157 \quad 20.6308] \text{ and}$$

$$G = [-0.0574 \quad 0.2684]^T.$$

The open loop response, response with state feedback gain obtained in simulation is shown in Fig. 2.

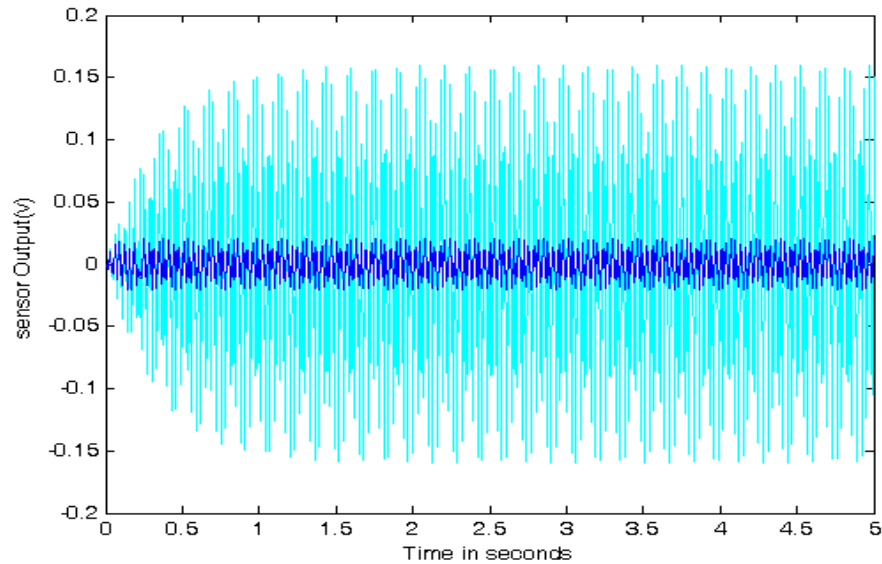


Fig. 2. Response to excitation at first natural frequency: - uncontrolled and controlled with state feedback gain.

The periodic output feedback gain obtained by solving equation (11) is

$$K = [48.6133 \quad 24.5878 \quad -5.6442 \quad -35.0216]$$

The open loop response, response with periodic output feedback gain obtained in simulation is shown in Fig. 3.

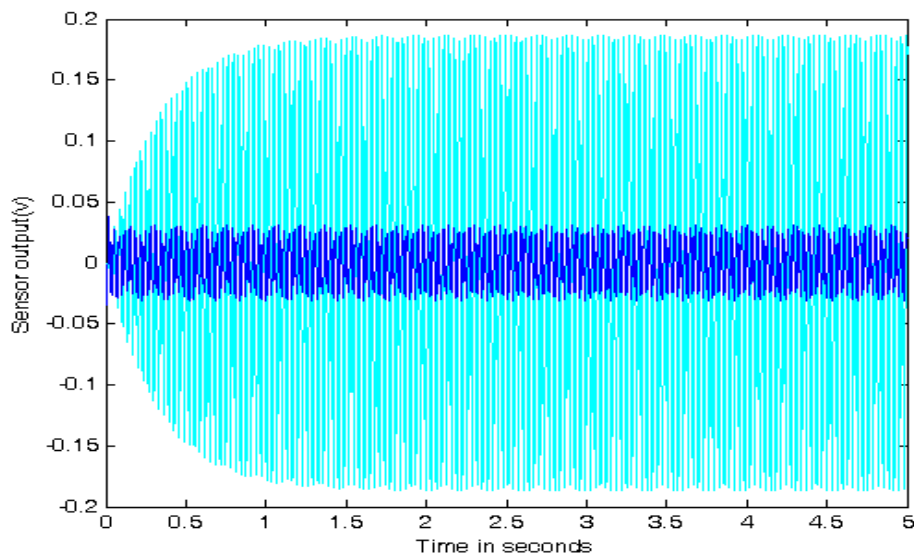


Fig. 3. Response to excitation at first natural frequency: - uncontrolled and controlled with Periodic output feedback gain.

5. Experimental Implementation Using Microcontroller

The periodic output feedback controller designed in section 4 is experimentally evaluated for its performance in suppressing the first vibration mode of smart cantilever beam using KEIL software.

The experimental set up with microcontroller (AT89C51) interface for implementing the controller is shown in Fig. 4. A sinusoidal excitation with first natural frequency and amplitude of 5V peak to peak is applied to the disturbance actuator which makes the beam to vibrate at resonance. The sensor output is fed to the piezo sensing system which consists of high quality charge to voltage signal conditioning amplifier with variable gain. The conditioned piezosensor signal is given as analog input to the level shifter for shifting the negative cycle to positive which is sampled at τ s by sample and hold and applied to Analog to Digital converter (ADC). The control signal is generated in microcontroller (AT89C51) as per the equation (11) and is applied as input to the Digital to Analog converter (DAC). The output of the DAC is connected to actuator via piezo actuation system. The uncontrolled and controlled response is shown in Fig. 5. In Fig. 5. initially the control signal is not applied latter the control is switched ON which suppresses the vibration.

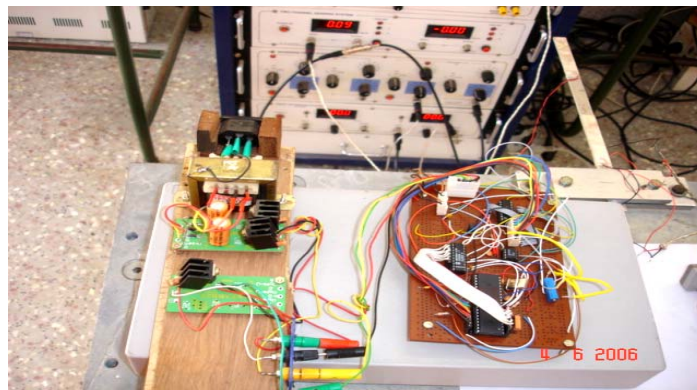


Fig. 4. Experimental set up with microcontroller interface.

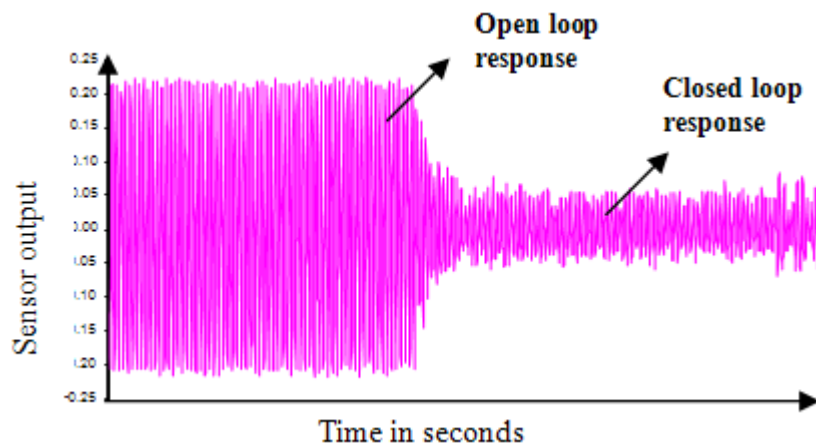


Fig. 5. Response to excitation at first natural frequency: - uncontrolled and controlled with Periodic output feedback gain (Experimental).

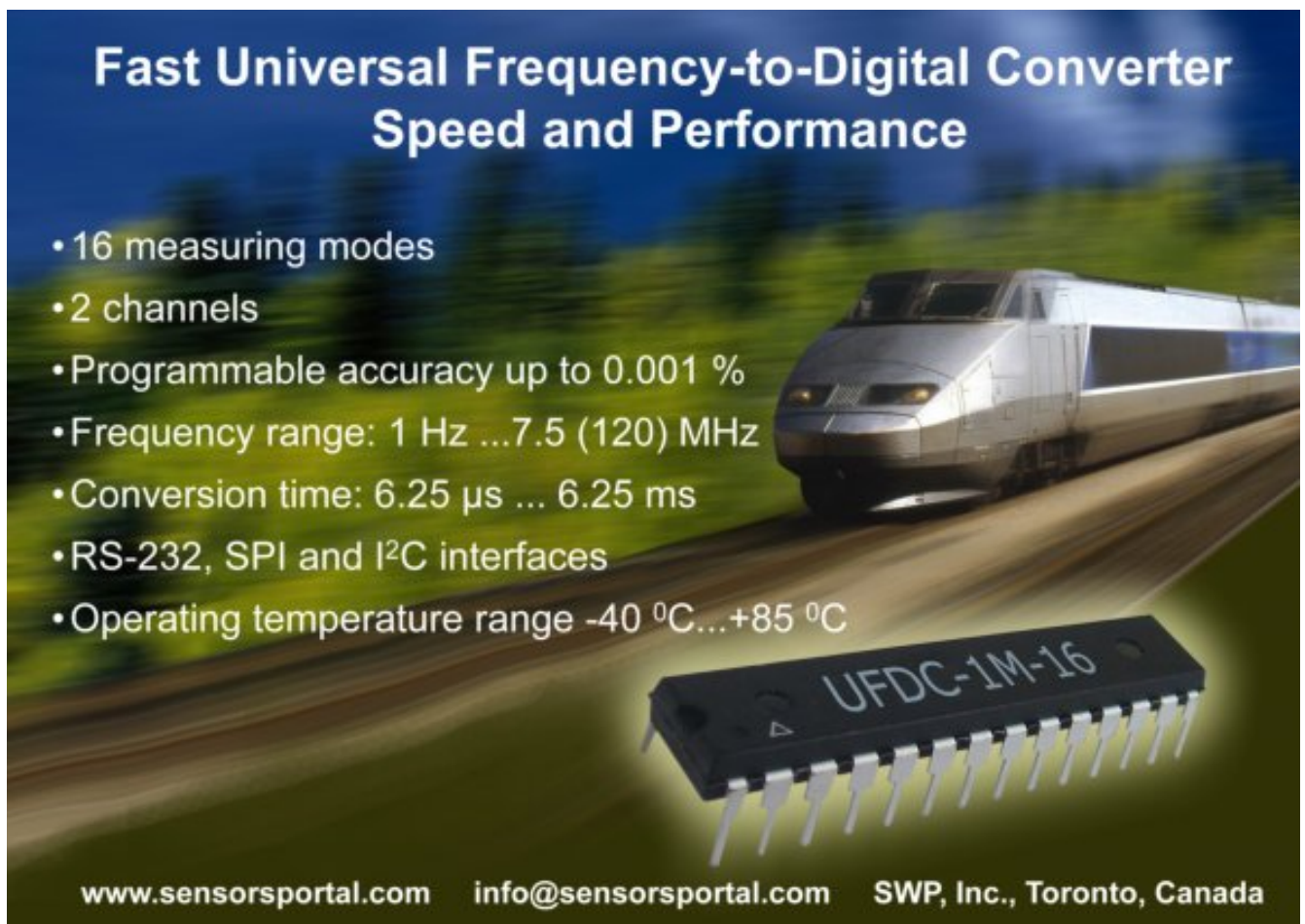
6. Conclusion

A periodic output feedback controller has been designed from the state feedback gain to control the first mode vibration of a cantilever beam using piezo actuator. The simulation and experimental results demonstrate the performance of the controller for vibration suppression. The hardware used for implementing the controller is very simple and cost effective.

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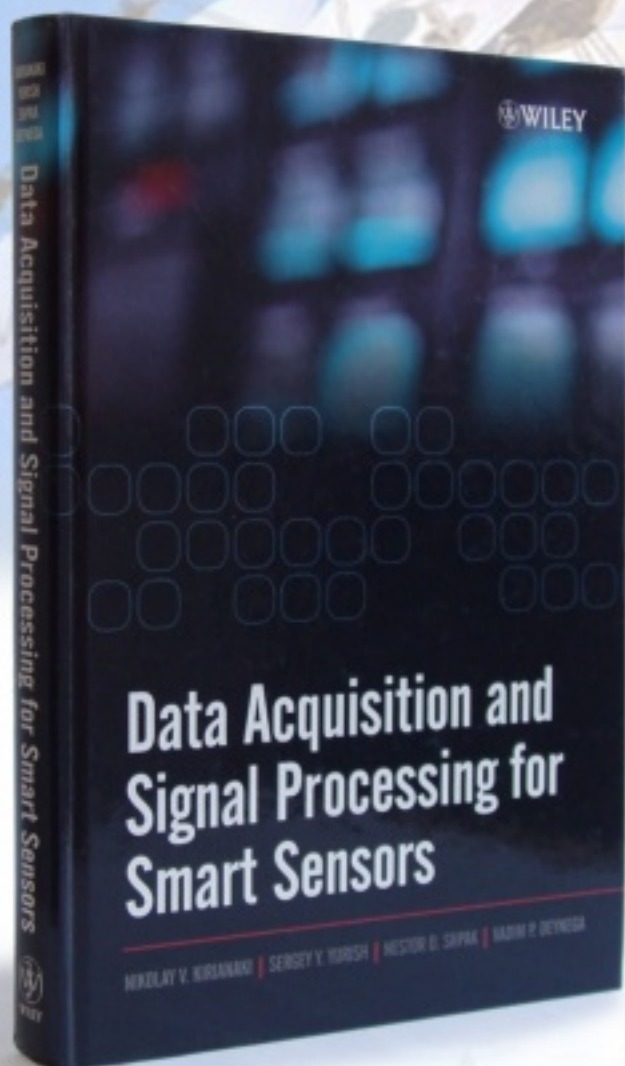
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