

Robust H_∞ Control Design of NCS

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Abstract: Some unknown elements always exist in the analysis process for the control systems, such as unmodeled dynamics, parametric uncertainties, change of the operating environment, model reduction and linearization approximations, etc., or external disturbance. So it is significative to study the disturbance process or the uncertain systems. The emergence and the development of the robust control theory were just in such environment, and it is becoming an important research field of the control theory and its practice applications. To address instability and jump degeneration of linear network control system with time-delay and packet dropout, and considering uncertainties of network control systems model and external disturbance, the paper presents network control systems delay-dependent stochastic stability and Linear matrix inequalities (LMI) conditions by introducing Lyapunov-Krasovskii functional and relaxation matrix variable. The paper proposes the network control system delay-dependent stochastic stability and disturbance attenuation LMI conditions and robust H_∞ control system perturbation attenuation performance analysis. By using simple mathematical derivation, solving two Riccati equations, we can be sub-optimal control solution. Finally, the simulation example can be found robust stability, simple and effective. *Copyright © 2014 IFSA Publishing, S. L.*

Keywords: Leave linear networked control system, H_∞ control, Riccati equation, Disturbance attenuation, Riccati equation method.

1. Introduction

The time-delay of the NCS is a hot topic at present. Considering the feature of the network, the delay may be constant, random, bounded or unbounded. Literature [1-3] reduces the random delay of the controlled system's forward path and feedback channel through the algorithm of the predictive control. Literature [4, 5] uses Lyapunov-Krasovskii function and LMI to get the stability condition of the time-delay. Literature [6] divides the delay into definite and continuous change parts, aiming at the uncertain system's robust stability feature with uncertain input latency, a sufficient stability condition of the system is offered through

Lyapunov function. Literature [7-12] considers the Markov random delay of the system, gives a more general continuous stochastic model of the NCS. Based on this, the stabilization of the system's robust H_∞ is researched through Lyapunov function, and a sufficient condition of the stochastic stability is offered [13].

In reference to the above references, the NCS with random delay and packet loss is researched in this paper. Through the algorithm of the random Lyapunov-Krasovskii functional and relaxation matrix variable, the LMI condition of the networked delay based on stochastic stability and disturbance attenuation is given [14]. Meanwhile, considering the uncertainties and external disturbance, the improved

2-Riccati equation is adopted to design the H_∞ controller.

2. Issue Description

Considering a state equation of a NCS shown as:

$$\begin{aligned} \dot{x} &= Ax + B_1w + B_2u \\ z &= C_1x + D_{11}w + D_{12}u, \\ y &= C_2 + D_{21}w + D_{22}u \end{aligned} \quad (1)$$

where $u(t) \in R^r$ is the input variable, y is the observed quantity, w is the external input variable, and z is the controlled output variable. In order to make Eq. 1 simpler, the coefficient matrix of the controlled plant is marked as T .

$$T = \begin{bmatrix} A & B_1 & B_2 \\ C_1 & D_{11} & D_{12} \\ C_2 & D_{21} & D_{22} \end{bmatrix}, \quad (2)$$

The following assumptions are made:

The sampling period is set as T . And the sensor adopts the time-driven approach, the controller and actuator adopt the event-driven approach [15].

The delay from the sensor to the controller is bounded random delay, and the status information $x_k - t_{rk}(r_k, k \geq 0)$ is a limited Markov chain, $S = \{1, 2, \dots, s\}$, $\Pi = [\pi_{ij}]$ is transition probability matrix, and

$$\begin{aligned} P[r_{k+1} = j, r_k = i] &= \pi_{ij} \\ \forall i, j \in S \end{aligned}$$

where

$$\pi_{ij} \geq 0, i \neq j; \sum_{j=1, j \neq i}^s \pi_{ij} = 1 - \pi_{ii}.$$

3. Main Results

3.1. Definition

Definition 1 [5] is for all $w_k \in l^2, w \neq 0$, wherein

$$l^2 = \left\{ a_k, k \geq 0 \mid \sum_{k=0}^{\infty} \|a_k\|^2 < \infty \right\},$$

the jump system is random and stable, and the controlled output $\{z_k\}$ shall satisfy

$$\|z\|_2 < \gamma \|w\|_2$$

where

$$\|z\|_2 = \left[\sum_{k=0}^{\infty} z_k^T z_k \right]^{1/2}, \gamma > 0$$

is the disturbance attenuation performance level, then the jump system is stochastic stable with γ attenuation feature.

Definition 2 For

$$w_k \in l^2, w \neq 0,$$

where

$$l^2 = \left\{ a_k, k \geq 0 \mid \sum_{k=0}^{\infty} \|a_k\|^2 < \infty \right\},$$

the jump system is stochastic stable, and the controlled output $\{z_k\}$ satisfy

$$\|z\|_2 < \gamma \|w\|_2,$$

where

$$\|z\|_2 = \left[\sum_{k=0}^{\infty} z_k^T z_k \right]^{1/2}, \gamma > 0$$

is the disturbance attenuation level, then the jump system is random and stable and featured with γ attenuation feature[16].

3.2. NCS Robust H_∞ Disturbance Attenuation Analysis and Controller Design

3.2.1. H_∞ Disturbance Attenuation Analysis

Theorem 1[6]: Concerning the random delay

$$\tau_m \leq \tau_i \leq \tau_M, i \in S,$$

if the matrix

$$P_i > 0, Q_1 > 0, Q_2 > 0, T_i = \begin{bmatrix} T_{1i} & T_{2i} & T_{3i} \end{bmatrix}$$

exists, H_i, N_i shall meet the following LMI:

$$\psi_i = \begin{bmatrix} \Theta_i + \gamma^{-1} C_i^T C_i & * \\ \gamma^{-1} D_2^T C_i + B_2^T T_i & \gamma^{-1} D_2^T D_{2i} - \mathcal{H} \end{bmatrix} < 0, \quad (3)$$

In the sum form

$$C_i = \begin{bmatrix} C_1 & D_{1i} & 0 \end{bmatrix},$$

concerning the linear jump system and given disturbance attenuation level γ , the system is featured with γ disturbance attenuation feature, then for all

$$w_k \in l^2, w \neq 0 : \|z\|_2 < \gamma \|w\|_2.$$

Proof : select the following Lyapunov functional:

$$V(x_k, r_k) = V_1(x_k, r_k) + V_2(x_k, r_k) + V_3(x_k, r_k) + V_4(x_k, r_k).$$

where

$$V_1(x_k, r_k) = x_k^T P_k x_k$$

$$V_2(x_k, r_k) = \sum_{l=k-\tau_1}^{k-1} x_l^T Q_1 x_l$$

$$V_3(x_k, r_k) = \sum_{\theta=-\tau_1}^{-1} \sum_{l=k+\theta}^{k-1} \delta_l^T Q_2 x_l$$

$$V_4(x_k, r_k) = (1-\pi_m) \sum_{\theta=-\tau_{i^*}+1}^{-\tau_m+1} \sum_{l=k+\theta-1}^{k-1} \{x_l^T Q_1 x_l + (l+1-k-\theta) \delta_l^T Q_2 \delta_l\}$$

then

$$2\varepsilon_k^T T_i^T \left\{ A_{si} x_k - \delta_k - B_{li} \sum_{l=k-\tau_1}^{k-1} \delta_l + B_2 w_k \right\} = 0$$

where

$$\varepsilon_k = \begin{bmatrix} x_k^T & x_{k-\tau_1}^T & \delta_k^T \end{bmatrix}^T$$

$$x_{k-\tau_1} = x_k - \sum_{l=k-\tau_1}^{k-1} \delta_l$$

$$\delta_l = x_{k+1} - x_l, A_{si} = A_i + B_{li} - I$$

where T_i is a matrix with certain dimensions.

From Eq.4, we can obtain

$$E[V(x_{k+1}, \tau_{k+1}) | F_k] - v(x_k, \tau_k) \leq \varepsilon_k^T \Theta \varepsilon_k + 2\varepsilon_k^T T_i^T B_2 w_k.$$

Assuming the zero initial condition, that is,

$$x_k = 0, k = -\tau_M, -\tau_M + 1, \dots, -1,$$

and the definition

$$J_N = \gamma^{-1} \|z\|_2^2 - \gamma \|w\|_2^2 = E \left[\sum_{j=0}^{N-1} (\gamma^{-1} z_j^T z_j - \gamma w_j^T w_j) \right].$$

For

$$V_0(\phi, \tau_0) = 0,$$

there are

$$E[V_N(x_N, r_N)] = E \left[\sum_{j=0}^{N-1} V_{k+1}(x_{k+1}, r_{k+1}) - V_k(x_k, r_k) \right] > 0$$

therefore we can get

$$\begin{aligned} J_N &= E \left[\sum_{j=0}^{N-1} V_{k+1}(x_{k+1}, r_{k+1}) - V_k(x_k, r_k) \right] + \gamma^{-1} z_k^T z_k - \gamma w_k^T w_k \\ &\quad - E[V_N(x_N, r_N)] \\ &\leq E \left[\sum_{j=0}^{N-1} V_{k+1}(x_{k+1}, r_{k+1}) - V_k(x_k, r_k) \right] + \gamma^{-1} z_k^T z_k - \gamma w_k^T w_k \\ &= \sum_{k=0}^{N-1} \eta_k^T \Psi_i \eta_k \end{aligned}$$

where

$$\eta_k = \begin{bmatrix} \xi_k^T & w_k^T \end{bmatrix}^T.$$

Then,

$$\sum_{k=0}^{N-1} \eta_k^T \Psi_i \eta_k < 0,$$

and for any nonzero

$$w_k \in l^2(0, \infty), z \in l^2(0, \infty),$$

there is

$$\|z\|_2 < \gamma \|w\|_2.$$

According to the definition 2, the theorem 1 can be proved.

3.2.2. Design of Status Feedback Controller

H_∞ design method can be roughly divided into two categories. The first category is the analytical solution based on function approximation theory; the second category is seeking the second-best solution through the analytical method, then relying on the repeated iteration to close to the optimal solution. The paper adopts the improved 2-Riccati equation belonging to the second category, and here mainly

aims at the formal standard H_∞ control issue. The method only needs to solve two algebraic Riccati equations, and it is a design method for the controller with a more application [17-21].

Before designing the H_∞ controller, the controlled object in the issue description shall be made the following assumptions: (A, B_2) can be calm, and (A, C_2) can be detected;

- 1) $D_{12} = \begin{bmatrix} 0 \\ I_p \end{bmatrix}$, and $D_{21} = \begin{bmatrix} 0 & I_q \end{bmatrix}$,
 $D_{11} = \begin{bmatrix} D_{1111} & D_{1112} \\ D_{1121} & D_{1122} \end{bmatrix}$, $D_{1111} \in R^{(m-p) \times (r-q)}$, $D_{1122} \in R^{p \times q}$
- 2) $\text{rank} \begin{bmatrix} -j\omega I + A & B_2 \\ C_1 & D_{12} \end{bmatrix} = n + p$
 $\text{rank} \begin{bmatrix} -j\omega I + A & B_1 \\ C_2 & D_{21} \end{bmatrix} = n + q, \forall \omega \in R$
- 3) $D_{22} = 0$

If the stable solution X_∞ and Y_∞ for the following algebraic Riccati equation exist, namely

$$X_\infty = \text{Ric} \begin{bmatrix} A - BR^{-1}D_{*1}^T C_1 & -BR^{-1}B^T \\ -C_1^T C_1 + C_1^T D_{*1} R^{-1} D_{*1}^T C_1 & -A^T + C_1^T D_{*1} R^{-1} B^T \end{bmatrix}$$

$$Y_\infty = \text{Ric} \begin{bmatrix} A^T - C^T \tilde{R}^{-1} D_{*1} B_1^T & -C^T \tilde{R}^{-1} C \\ -B_1 B_1^T + B_1 D_{*1}^T \tilde{R}^{-1} D_{*1} B_1^T & -A + B_1 D_{*1}^T \tilde{R}^{-1} C \end{bmatrix}$$

The matrix F and H are defined as

$$F = \begin{bmatrix} F_{11} \\ F_{12} \\ F_2 \end{bmatrix} = -R^{-1} [D_{*1}^T C_1 + B^T X_\infty]$$

$$H = [H_{11} \quad H_{12} \quad H_2] = -[B_1 D_{*1}^T + Y_\infty C^T] \tilde{R}^{-1}$$

If the above controlled plant in theorem 2[7] meets the above assumptions, then a closed-loop stable controller exists and the sufficient and necessary condition meeting for $\|\phi(s)\|_\infty < \gamma$ is satisfying the following four conditions[22-25]:

- 1) $\max(\bar{\sigma} [D_{1111}, D_{1112}], \bar{\sigma} [D_{1111}^T, D_{1121}^T]) < \gamma$;
- 2) $X_\infty \geq 0$;
- 3) $Y_\infty \geq 0$;
- 4) $\rho(X_\infty, Y_\infty) < \gamma^2$.

where $\bar{\sigma}(\cdot)$ represents the maximum singular value of the matrix, and $\rho(\cdot)$ represents the maximum eigenvalue of the matrix.

When the above conditions are satisfied, the H_∞ controller is

$$K = F_l(K_a, S)$$

where $S \in BH_\infty^{p \times q}$ and K_a is expressed as

$$K_a = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} = \begin{bmatrix} \hat{A} & \hat{B}_1 & \hat{B}_2 \\ \hat{C}_1 & \hat{D}_{11} & \hat{D}_{12} \\ \hat{C}_2 & \hat{D}_{21} & 0 \end{bmatrix},$$

where

$$\hat{D}_{11} = -D_{1121} D_{1111}^T (\gamma^2 I - D_{1111} D_{1111}^T)^{-1} D_{1112} - D_{1122}$$

$$\hat{B}_2 = (B_2 + H_{12}) \hat{D}_{12}$$

$$\hat{C}_2 = -\hat{D}_{21} (C_2 + F_{12}) Z$$

$$\hat{B}_1 = -H_2 + \hat{B}_2 \hat{D}_{12}^{-1} \hat{D}_{11}$$

$$\hat{C}_1 = F_2 Z + \hat{D}_{11} \hat{D}_{21}^{-1} \hat{C}_2$$

$$\hat{A} = A + HC + \hat{B}_2 \hat{D}_{12}^{-1} \hat{C}_1$$

$$Z = (I - \gamma^2 Y_\infty X_\infty)^{-1}$$

where

$$\hat{D}_{12} \in R^{p \times q}, \hat{D}_{21} \in R^{q \times p}$$

$$\hat{D}_{12} \hat{D}_{12}^T = I - D_{1121} (\gamma^2 I - D_{1111}^T D_{1111})^{-1} D_{1121}^T$$

$$\hat{D}_{21}^T \hat{D}_{21} = I - D_{1112}^T (\gamma^2 I - D_{1111} D_{1111}^T)^{-1} D_{1112}$$

Therefore, to meet the assumptions of Theorem 2 standard control problem, as long as solving two algebraic Riccati equation, you can find all of the sub-controller optimal control problems [26-31].

4. Simulation Example

An uncertain network control system is established here, and the realization of the controlled object's state space is:

$$A = \begin{bmatrix} -22 & 0 & 0 \\ -164 & -0.43 & 0 \\ 0 & -1 & -0.001 \end{bmatrix}, B_1 = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}, B_2 = \begin{bmatrix} 4.2 \\ 0 \\ 0 \end{bmatrix}$$

$$C_1 = \begin{bmatrix} 0 & -0.1 & 3.5 \\ 0 & 0 & 0 \\ -0.3 & -0.01 & 0 \end{bmatrix}, C_2 = [0 \quad -1 \quad 0]$$

$$D_{11} = \begin{bmatrix} 0.1 \\ 0 \\ 0 \end{bmatrix}, D_{12} = \begin{bmatrix} 0 \\ 0.01 \\ 0 \end{bmatrix}, D_{21} = [1], D_{22} = [0]$$

Through solving Riccati equations by MATLAB robust control toolbox, the controller can be obtained

$$K = \frac{356(s+20)(s+0.43)}{s(s^2+205s+11906)}, \quad (6)$$

By the MTLAB simulation, the controller's frequency feature is shown as Fig. 2:

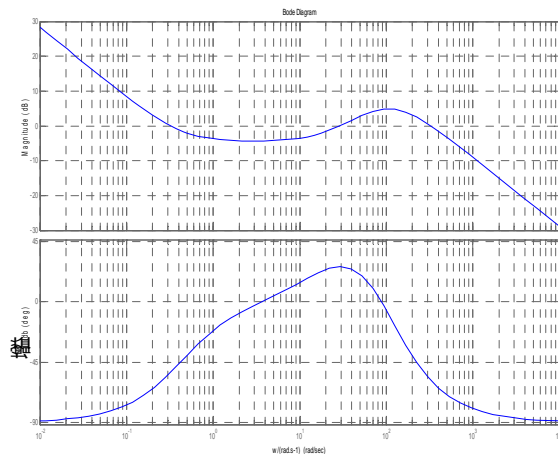


Fig. 2. The frequency feature of the controller.

It's seen that the sink low gain appears at the point $w=3.3$ rad/s from Fig. 2. The gain can effectively suppress the influence of the interference.

4. Conclusion

H_∞ robust stability is designed of the NCS with random delay and packet loss through the improved Riccati equations. It only uses a simple mathematical derivation to gain the H_∞ sub-optimal control solution. From the simulation example, it's seen that it has a great robust stability and it's simple and effective which has the certain practical value.

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