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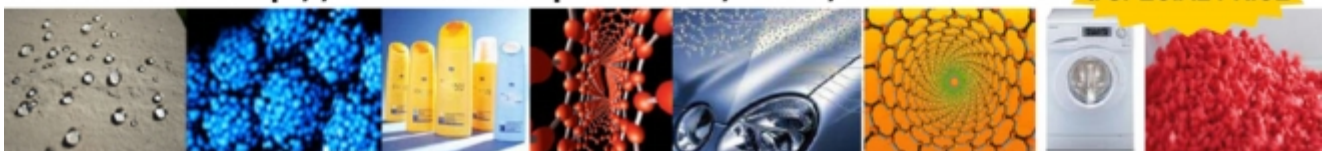
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Harmonic Response of Magneto-electro-elastic Sensors Bonded to Cylindrical Shells

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Abstract: This paper deals with semi analytical finite element formulation for coupled magneto-electro-elastic sensor bonded to a mild steel cylindrical shell. The cylinder is subjected to harmonically varying internal pressure with clamped free and clamped-clamped boundary condition. Numerical results are presented for the first three axial modes associated with the axisymmetric mode of the shell with different sensor locations. The sensor response is controlled mainly by its radial displacement in all the modes. The third mode response becomes significant when the sensor is placed at the free end of the mild steel cylinder for clamped free boundary condition. *Copyright © 2010 IFSA.*

Keywords: Magneto-electro-elastic, Sensor, Harmonic response, Semi analytical finite element

1. Introduction

Composite materials that possess simultaneously piezoelectric, piezomagnetic and magneto electric effects are classified as Magneto-electro-elastic (MEE) materials. The composite consisting of piezoelectric phase shows a coupling between mechanical and electric field where as the piezomagnetic phase shows the coupling between mechanical and magnetic field. Magneto-electric coupling effect which is absent in the constituent phases is also exhibited by these class of magneto-electro-elastic materials. On application of either mechanical, electric or magnetic loads, these materials will respond in such a way to convert one form of energy into another. These materials are widely used in acoustic devices, magnetic field probes, medical ultrasonic imaging, sensors and actuators etc. Harmonic response analysis helps to predict the sustained dynamic behavior of the structure, thus enabling to predict whether the structure will overcome resonance, fatigue and other

harmful effects of forced vibration. Response characteristics of MEE sensors under dynamic loading will help to determine the best operating conditions of MEE devices which in turn will lead to emerging areas for application of magneto-electro-elastic materials as sensors and actuators.

Fibrous composites consisting of piezomagnetic cobalt iron oxide $CoFe_2O_4$ matrix reinforced by piezoelectric barium titanate $BaTiO_3$ fibers (Buchanan, 2004) are analyzed for the sensory response. The composite is transversely isotropic with plane of symmetry oriented in the radial direction. Aboudi (2001) has employed a homogenization method assuming that the composites have a periodic structure, for predicting the effective moduli of magneto-electro-elastic composites. Ramirez *et al* (2006) presented approximate solution to a free vibration problem of a two dimensional MEE laminate assuming perfect bonding between each interface. Analytical solution for transient response of MEE hollow cylinder was presented by Hou *et al* (2004) where plain strain condition with axisymmetric loading was used so that radial displacement only is considered to derive the solution. Transient responses of displacements, stresses, electric and magnetic potentials, electric displacements, magnetic induction are obtained by the study. Dai *et al* (2006) has presented an analytical solution for magneto-thermo-electro-elastic transient response of a piezoelectric hollow cylinder placed in an axial magnetic field subjected to arbitrary thermal shock, mechanical load and transient electric excitation. Sirohi *et al* (2000) investigated the piezoelectric strain sensor in which strain is measured in terms of charge developed by direct piezoelectric effect. Huang *et al* (2000) examined the dynamic electromechanical response of piezoelectric sensors and actuators which are modeled as rectangular plate and the variation of electric potential, stresses and electric displacements across the thickness were evaluated. Galopin *et al* (2008) has done finite element modeling of magneto electric sensors and the magneto electric effect stemming from piezoelectric and magnetostrictive composite was studied. Daga *et al* (2009) has studied the behavior of MEE sensors bonded to beam under transient mechanical loading.

This paper deals with harmonic response of magneto-electro-elastic sensor bonded to an axisymmetric cylindrical shell. The sensor is bonded on the outer surface of a shell structure. Semi analytical finite element method is used to model the entire structure. Dynamic response of the sensor is studied when the cylinder is subjected to harmonically varying internal pressure. Numerical studies are carried out for clamped-free and clamped-clamped boundary conditions with the sensor placed at different locations on the top surface of the cylinder. These studies will be highly useful when we use MEE sensors and actuators for active vibration control of structures. Ansys 10.1 is used to validate the computer code developed for the study. Ansys cannot model fully coupled magneto-electro-elastic materials but it can model piezoelectric material *PZT-5* which is used to compare with the results of the code.

2. Constitutive Equations

The constitutive equations for the MEE medium relating stress σ_j , electric displacement D_l and magnetic induction B_l to strain S_k , electric field E_m and magnetic field H_m , exhibiting linear coupling between magnetic, electric and elastic field can be written as (Daga *et al* (2008))

$$\sigma_j = C_{jk}S_k - e_{jm}E_m - q_{jm}H_m \quad (1)$$

$$D_l = e_{lj}S_k + \varepsilon_{lm}E_m + m_{lm}H_m \quad (2)$$

$$B_l = q_{lj}S_k + m_{lm}E_m + \mu_{lm}H_m, \quad (3)$$

where C_{jk} , ε_{lm} and μ_{lm} are elastic, dielectric and magnetic permeability coefficients respectively and e_{ij} , q_{ij} and m_{lm} are the piezoelectric, piezomagnetic and magnetoelectric material coefficients. Here $j, k = 1, \dots, 6$ and $l, m = 1, \dots, 3$.

2.2. Finite Element Modeling of the Shell

In the axi-symmetric cylindrical shell, the geometry and material properties do not vary along circumferential (θ) direction and semi analytical finite element approach can be used for a simplified solution. The displacements, electric scalar potential and magnetic scalar potential are expressed using Fourier series in the circumferential direction.

$$u_r = \sum u_r^n \cos n\theta \quad (2.1)$$

$$u_\theta = \sum u_\theta^n \sin n\theta \quad (2.2)$$

$$u_z = \sum u_z^n \cos n\theta \quad (2.3)$$

$$\phi = \sum \phi^n \cos n\theta \quad (2.4)$$

$$\psi = \sum \psi^n \cos n\theta, \quad (2.5)$$

where u_r, u_θ, u_z are the radial, circumferential and axial displacements, ϕ and ψ are the electric and magnetic scalar potentials respectively.

The displacements $\{u\} = \{u_r, u_\theta, u_z\}^T$, electric potential (ϕ) and magnetic potential (ψ) within the element can be expressed in terms of suitable shape functions and the corresponding nodal quantities.

$$\{u\} = [N_u] \{u^e\}; \phi = [N_\phi] \{\phi^e\}; \psi = [N_\psi] \{\psi^e\} \quad (3)$$

The strains can be related to the nodal degree of freedom by the following expression

$$\{S\} = [B_u] \{u^e\}, \quad (4)$$

where $[B_u]$, the strain displacement matrix can be written as

$$[B_u] = [L_u][N_u] \quad (5)$$

$$= \begin{bmatrix} \frac{\partial}{\partial r} & 0 & 0 \\ \frac{1}{r} & \frac{1}{r} \frac{\partial}{\partial \theta} & 0 \\ 0 & 0 & \frac{\partial}{\partial z} \\ 0 & \frac{\partial}{\partial z} & \frac{1}{r} \frac{\partial}{\partial \theta} \\ \frac{\partial}{\partial z} & 0 & \frac{\partial}{\partial r} \\ \frac{1}{r} \frac{\partial}{\partial \theta} & \frac{\partial}{\partial r} - \frac{1}{r} & 0 \end{bmatrix} \begin{bmatrix} N_1 & 0 & 0 & N_2 & 0 & 0 & N_3 & 0 & 0 & N_4 & 0 & 0 \\ 0 & N_1 & 0 & 0 & N_2 & 0 & 0 & N_3 & 0 & 0 & N_4 & 0 \\ 0 & 0 & N_1 & 0 & 0 & N_2 & 0 & 0 & N_3 & 0 & 0 & N_4 \end{bmatrix}$$

$$[B_u] = \begin{bmatrix} \frac{\partial N_1}{\partial r} & 0 & 0 & \dots \\ \frac{N_1}{r} & \frac{nN_1}{r} & 0 & \dots \\ 0 & 0 & \frac{\partial N_1}{\partial z} & \dots \\ 0 & \frac{\partial N_1}{\partial z} & -\frac{nN_1}{r} & \dots \\ \frac{\partial N_1}{\partial z} & 0 & \frac{\partial N_1}{\partial r} & \dots \\ -\frac{nN_1}{r} & \frac{\partial N_1}{\partial r} - \frac{N_1}{r} & 0 & \dots \end{bmatrix} \quad (6)$$

In the present formulation body forces, free charge density and free current density are absent. In the absence of free charge density, Gauss law can be reduced as $C.D = 0$ where D is the electric displacement vector. The electric potential f which satisfies the above relation is defined so that the electric field E can be written as $E = -Cf$. The relation between electric field (E_m) related to electric potential (ϕ) can be written as

$$E_r = -\frac{\partial \phi}{\partial r}, \quad E_\theta = -\frac{1}{r} \frac{\partial \phi}{\partial \theta}, \quad E_z = -\frac{\partial \phi}{\partial z} \quad (7)$$

The array of electric field vector is given by

$$\{E\} = \left\{ -\frac{\partial \phi}{\partial r} \quad -\frac{1}{r} \frac{\partial \phi}{\partial \theta} \quad -\frac{\partial \phi}{\partial z} \right\} \quad (8)$$

The electric field vector can be related to the electric potential as a nodal degree of freedom using the following expression as

$$\{E\} = [B_\phi] \{\phi^e\} \quad (9)$$

The derivative of shape function matrix $[B_\phi]$ matrix is given below as

$$[B_\phi] = [L_\phi][N_\phi]$$

$$= \begin{bmatrix} -\frac{\partial}{\partial r} \\ -\frac{1}{r} \frac{\partial}{\partial \theta} \\ -\frac{\partial}{\partial z} \end{bmatrix} [N_1 \quad N_2 \quad N_3 \quad N_4] \quad (10)$$

$$[B_\phi] = \begin{bmatrix} -\frac{\partial N_1}{\partial r} & -\frac{\partial N_2}{\partial r} & -\frac{\partial N_3}{\partial r} & -\frac{\partial N_4}{\partial r} \\ \frac{nN_1}{r} & \frac{nN_2}{r} & \frac{nN_3}{r} & \frac{nN_4}{r} \\ -\frac{\partial N_1}{\partial z} & -\frac{\partial N_2}{\partial z} & -\frac{\partial N_3}{\partial z} & -\frac{\partial N_4}{\partial z} \end{bmatrix} \quad (11)$$

The magnetic field is formulated using scalar potential approach. In the absence of free current density, Gauss law for magnetic field can be written as $\text{C} \cdot \mathbf{B} = 0$ where \mathbf{B} is the magnetic induction vector. The magnetic scalar potential ψ which satisfies the above relation is defined so that the magnetic field H can be written as $H = -\nabla \psi$. The magnetic field (H_m) related to magnetic potential (ψ) can be written as

$$H_r = -\frac{\partial \psi}{\partial r}, \quad H_\theta = -\frac{1}{r} \frac{\partial \psi}{\partial \theta}, \quad H_z = -\frac{\partial \psi}{\partial z} \quad (12)$$

The array of magnetic field vector is given by

$$\{H\} = \left\{ -\frac{\partial \psi}{\partial r} \quad -\frac{1}{r} \frac{\partial \psi}{\partial \theta} \quad -\frac{\partial \psi}{\partial z} \right\} \quad (13)$$

The magnetic field vector $\{H\}$ can be related to the magnetic potential as a nodal degree of freedom the following expression

$$\{H\} = [B_\psi] \{\psi^e\} \quad (14)$$

The derivative of shape function matrix $[B_\psi]$ matrix is given below as

$$[B_\psi] = [L_\psi][N_\psi]$$

$$= \begin{bmatrix} -\frac{\partial}{\partial r} \\ \frac{1}{r} \frac{\partial}{\partial \theta} \\ -\frac{\partial}{\partial z} \end{bmatrix} [N_1 \quad N_2 \quad N_3 \quad N_4] \quad (15)$$

$$[B_\psi] = \begin{bmatrix} -\frac{\partial N_1}{\partial r} & -\frac{\partial N_2}{\partial r} & -\frac{\partial N_3}{\partial r} & -\frac{\partial N_4}{\partial r} \\ \frac{nN_1}{r} & \frac{nN_2}{r} & \frac{nN_3}{r} & \frac{nN_4}{r} \\ -\frac{\partial N_1}{\partial z} & -\frac{\partial N_2}{\partial z} & -\frac{\partial N_3}{\partial z} & -\frac{\partial N_4}{\partial z} \end{bmatrix} \quad (16)$$

2.3. Evaluation of Elemental Matrices

The finite element equations for MEE cylinder can be written as

$$\begin{aligned}
 [M_{uu}^e] \{\ddot{u}^e\} + [K_{uu}^e] \{u^e\} + [K_{u\phi}^e] \{\phi^e\} + [K_{u\psi}^e] \{\psi^e\} &= \{F^e\} \\
 [K_{u\phi}^e]^T \{u^e\} - [K_{\phi\phi}^e] \{\phi^e\} - [K_{\phi\psi}^e] \{\psi^e\} &= \{G^e\} \\
 [K_{u\psi}^e]^T \{u^e\} - [K_{\phi\psi}^e]^T \{\phi^e\} - [K_{\psi\psi}^e] \{\psi^e\} &= \{M^e\}
 \end{aligned} \quad , \quad (17)$$

where F, G and M correspond to elemental load vectors of applied mechanical force, electric charge and magnetic current respectively.

Different elemental matrices in Equation (17) for n^{th} harmonic are defined as

$$\begin{aligned}
 [M_{uu}^e] &= P \int_A [N_u]^T [\rho] [N_u] r dr dz \\
 [K_{uu}^e] &= P \int_A [B_u]^T [c] [B_u] r dr dz \\
 [K_{u\phi}^e] &= P \int_A [B_u]^T [e] [B_\phi] r dr dz \\
 [K_{u\psi}^e] &= P \int_A [B_u]^T [q] [B_\psi] r dr dz \\
 [K_{\phi\phi}^e] &= P \int_A [B_\phi]^T [\varepsilon] [B_\phi] r dr dz \\
 [K_{\psi\psi}^e] &= P \int_A [B_\psi]^T [\mu] [B_\psi] r dr dz \\
 [K_{\phi\psi}^e] &= P \int_A [B_\phi]^T [m] [B_\psi] r dr dz,
 \end{aligned} \quad (18)$$

where $P = 2\pi$ for $n = 0$ and $P = \pi$ for $n > 0$, n is circumferential harmonic number.

When electric and magnetic loading are absent, using standard condensation techniques, the equivalent stiffness matrix $[K_{eq}]$ is derived by eliminating the electric potential (ϕ) and magnetic potential (ψ) from Equation (17). For harmonic mechanical loading equation (17) can be rewritten as

$$[M_{uu}] \{\ddot{u}\} + [K_{eq}] \{u\} = \{F e^{i\omega t}\}, \quad (19)$$

where

$$[K_{eq}] = [K_{uu}] + [K_{u\phi}] [K_{II}]^{-1} [K_{I}] + [K_{u\psi}] [K_{IV}]^{-1} [K_{III}], \quad (20)$$

where

$$\begin{aligned}
 [K_I] &= [K_{u\phi}]^T - [K_{\phi\psi}] [K_{\psi\psi}]^{-1} [K_{u\psi}]^T \\
 [K_{II}] &= [K_{\phi\phi}] - [K_{\phi\psi}] [K_{\psi\psi}]^{-1} [K_{\phi\psi}]^T \\
 [K_{III}] &= [K_{u\psi}]^T - [K_{\phi\psi}]^T [K_{\phi\phi}]^{-1} [K_{u\phi}]^T \\
 [K_{IV}] &= [K_{\psi\psi}] - [K_{\phi\psi}]^T [K_{\phi\phi}]^{-1} [K_{\phi\psi}]
 \end{aligned} \tag{21}$$

After evaluating the nodal displacements, the electric potential (ϕ) and magnetic potential (ψ) can be derived at each nodal points using the following equations

$$\text{Electric potential } \{\phi\} = [K_{II}]^{-1} [K_I] \{u\} \tag{22}$$

$$\text{Magnetic potential } \{\psi\} = [K_{IV}]^{-1} [K_{III}] \{u\} \tag{23}$$

3. Results and Discussions

3.1. Validation

A computer code has been developed to study the harmonic response of magneto-electro-elastic sensor bonded on the outer surface of a mild steel cylindrical shell while the cylinder is subjected to a harmonic pressuring load (Fig. 1). Constant damping ratio of 0.01 is assumed and full method is used as the solution technique. The study is carried out for axisymmetric model of the shell structure with $n=0$. The circumferential displacement (u_θ) will be suppressed when $n=0$ and the model will simplify to a 2D axisymmetric model.

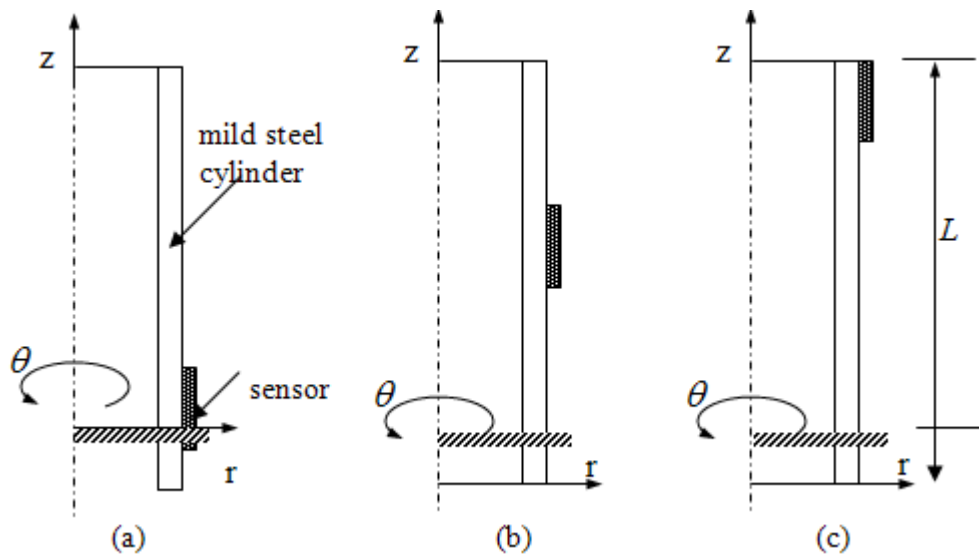


Fig. 1. Schematic diagram of a mild steel cylinder with sensor patch placed at (a) clamped end; (b) middle; and (c) free end.

The commercial finite element package Ansys 10.1 cannot model fully coupled magneto-electro-elastic materials but it can model piezoelectric materials. The present code is validated using piezoelectric material PZT-5 whose material properties (Chen *et al* (2007)) are given in Table 1. The dimensions of the cylinder used for the analysis are $L = 4.0\text{m}$, $R_i = 0.5\text{ m}$ and $R_o = 0.51\text{ m}$. The cylinder is subjected to a uniform internal pressure of 100 N/m^2 with clamped-free and clamped-clamped boundary condition.

Table 1. Material properties of PZT-5 and different volume fraction v_f of multiphase magneto-electro-elastic $\text{BaTiO}_3\text{-CoFe}_2\text{O}_4$ for radial plane of symmetry.

	0.0 v_f	0.2 v_f	0.4 v_f	0.6 v_f	0.8 v_f	1.0 v_f	PZT-5
Elastic constants							
C_{11}	269.5	240	220	190	170	162	86.85
C_{12}	170	145	125	110	100	78	54.01
C_{23}	173	146	125	110	100	77	50.77
$C_{22}=C_{33}$	286	250	225	200	175	166	99.2
$C_{44}=C_{66}$	45.3	45	45	45	50	43	21.1
Piezoelectric constants							
e_{11}	0	4.0	7.0	11.0	14.0	18.6	15.1
e_{12}	0	-2.0	-3.0	-3.5	-4.0	-4.4	-7.2
e_{35}	0	0	0	0	0	11.6	12.32
Dielectric constants							
e_{11}	0.093	2.5	5.0	7.5	10.0	12.6	1.5
$e_{22} = e_{33}$	0.08	0.33	0.8	0.9	1.0	11.2	1.53
Magnetic permeability constants							
m_{11}	1.57	1.33	1.0	0.75	0.5	0.1	0
$m_{22} = m_{33}$	-5.9	-3.9	-2.5	-1.5	-0.8	0.05	0
Piezomagnetic constants							
q_{11}	700	550	380	260	120	0	0
q_{12}	580	410	300	200	100	0	0
q_{35}	560	340	220	180	80	0	0
Magnetolectric constants							
m_{11}	0	2000	2750	2500	1500	0	0
m_{33}	0	2.8	4.8	6.0	6.8	0	0
Density							
r	5300	5400	5500	5600	5700	5800	7750

C_{jk} in 10^9N/m^2 , e_{ij} in C/m^2 , e_{im} in 10^{-9}C/Vm , q_{ij} in N/Am , m_{im} in $10^{-4}\text{Ns}^2/\text{C}^2$, m_{im} in 10^{-12}Ns/VC , r in kg/m^3

The radial displacement (u_r), axial displacement (u_z) and electric potential (ϕ) of a node on the sensor which gives maximum electric response is plotted in Fig. 2 using both the code and Ansys. The results are found to be in good agreement.

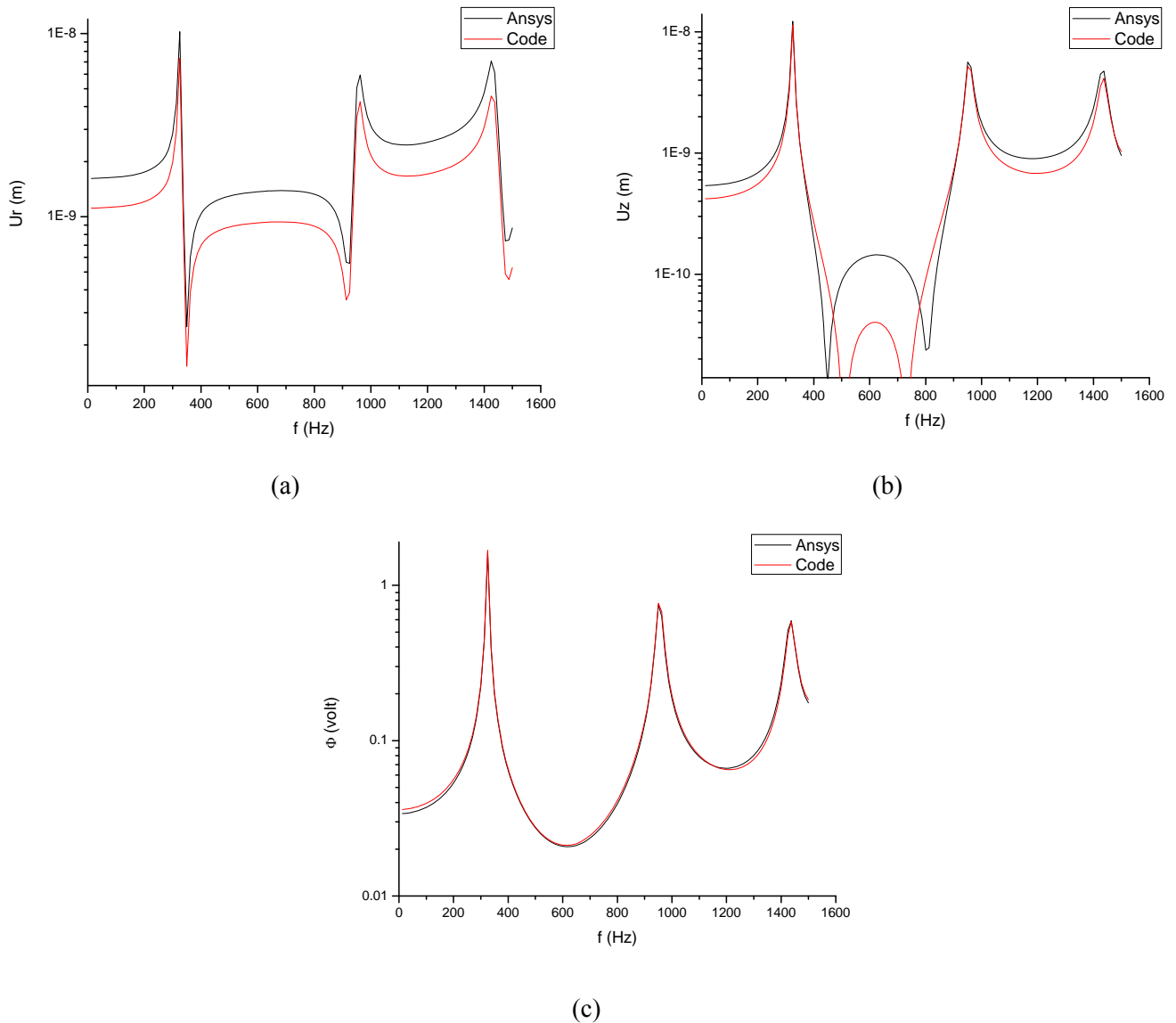


Fig. 2. Validation of the code for (a) radial displacement (u_r); (b) axial displacement (u_z); and (c) electric potential (ϕ).

3.2. Clamped-free Boundary Condition of the Shell

3.2.1. Sensor at Clamped End

The radial displacement (u_r), axial displacement (u_z), electric potential (ϕ) and magnetic potential (ψ) of a node on the sensor when the sensor is placed at the clamped end is shown in Fig. 3. The study is carried out for different volume fractions of $BaTiO_3$ in a composite of $BaTiO_3-CoFe_2O_4$ as shown in Table 1. It is seen that the electric potential (ϕ) is maximum when $\nu f=0.2$ which can be attributed to the induced strain because of the high elastic constants for $\nu f=0.2$. The magnetic potential (ψ) is maximum when $\nu f=0.0$ which corresponds to pure piezomagnetic composite having maximum value of piezomagnetic coupling constants. The first mode is dominating the response when the sensor is placed at the clamped end.

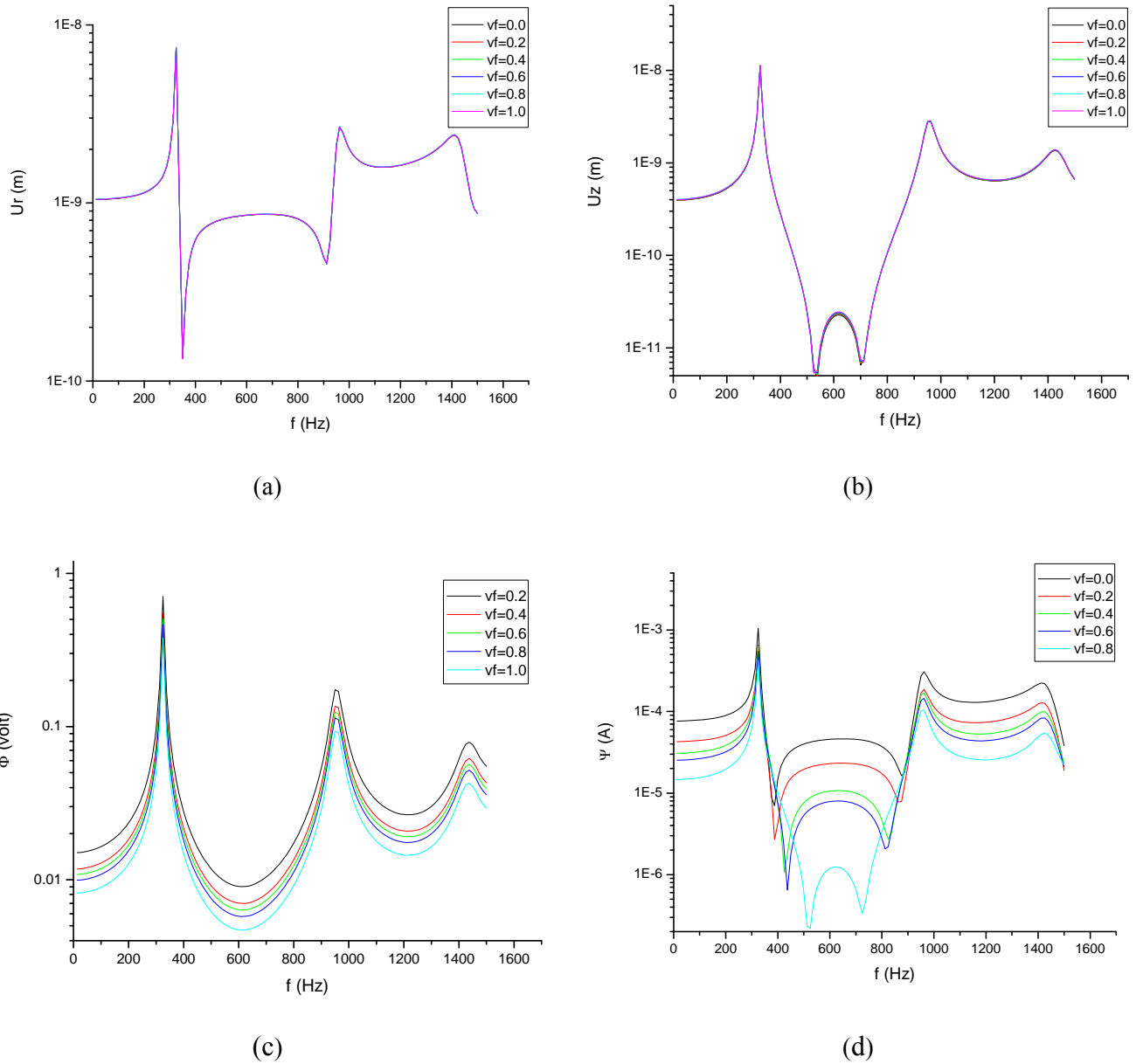


Fig. 3. (a) Radial displacement (u_r); (b) axial displacement (u_z); (c) electric potential (ϕ); and (d) magnetic potential (ψ) when sensor at clamped end.

3.2.2. Sensor at Middle

Fig. 4 shows the radial displacement (u_r), axial displacement (u_z), electric potential (ϕ) and magnetic potential (ψ) of a node on the sensor when the sensor is placed at the middle of the cylinder. The absolute value of response decreases and the response is controlled by the radial component of displacement when the sensor is placed at the middle of the shell.

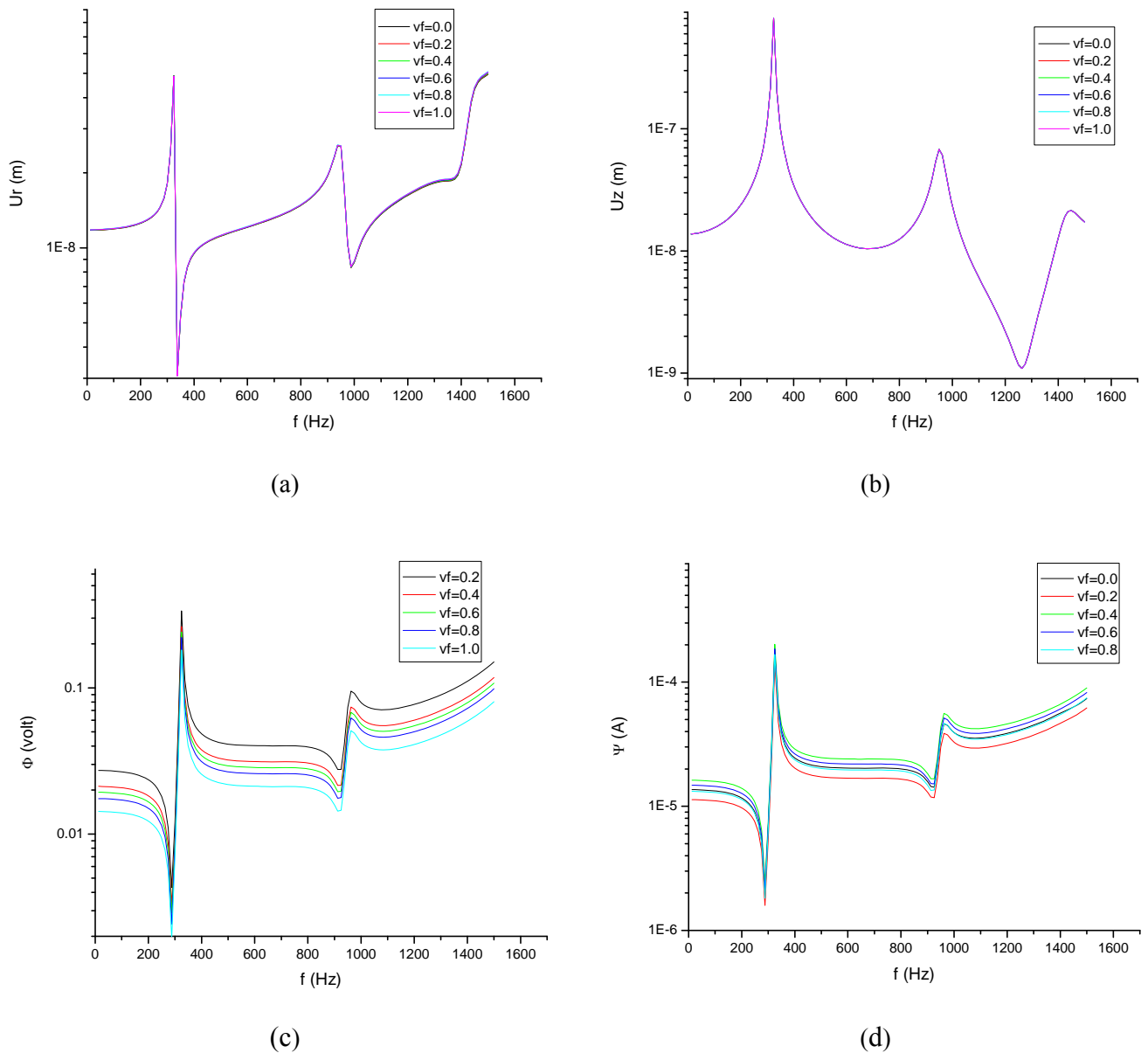


Fig. 4. (a) Radial displacement (u_r); (b) axial displacement (u_z); (c) electric potential (ϕ); and (d) magnetic potential (ψ) when sensor at middle.

3.2.3. Sensor at Free End

The radial displacement (u_r), axial displacement (u_z), electric potential (ϕ) and magnetic potential (ψ) of a node on the sensor when sensor is placed at the free end is shown in Fig. 5. The radial displacement is high during the third axisymmetric mode. The electric and magnetic potential is high for the third mode and it can be concluded that the response is significantly controlled by the radial displacement.

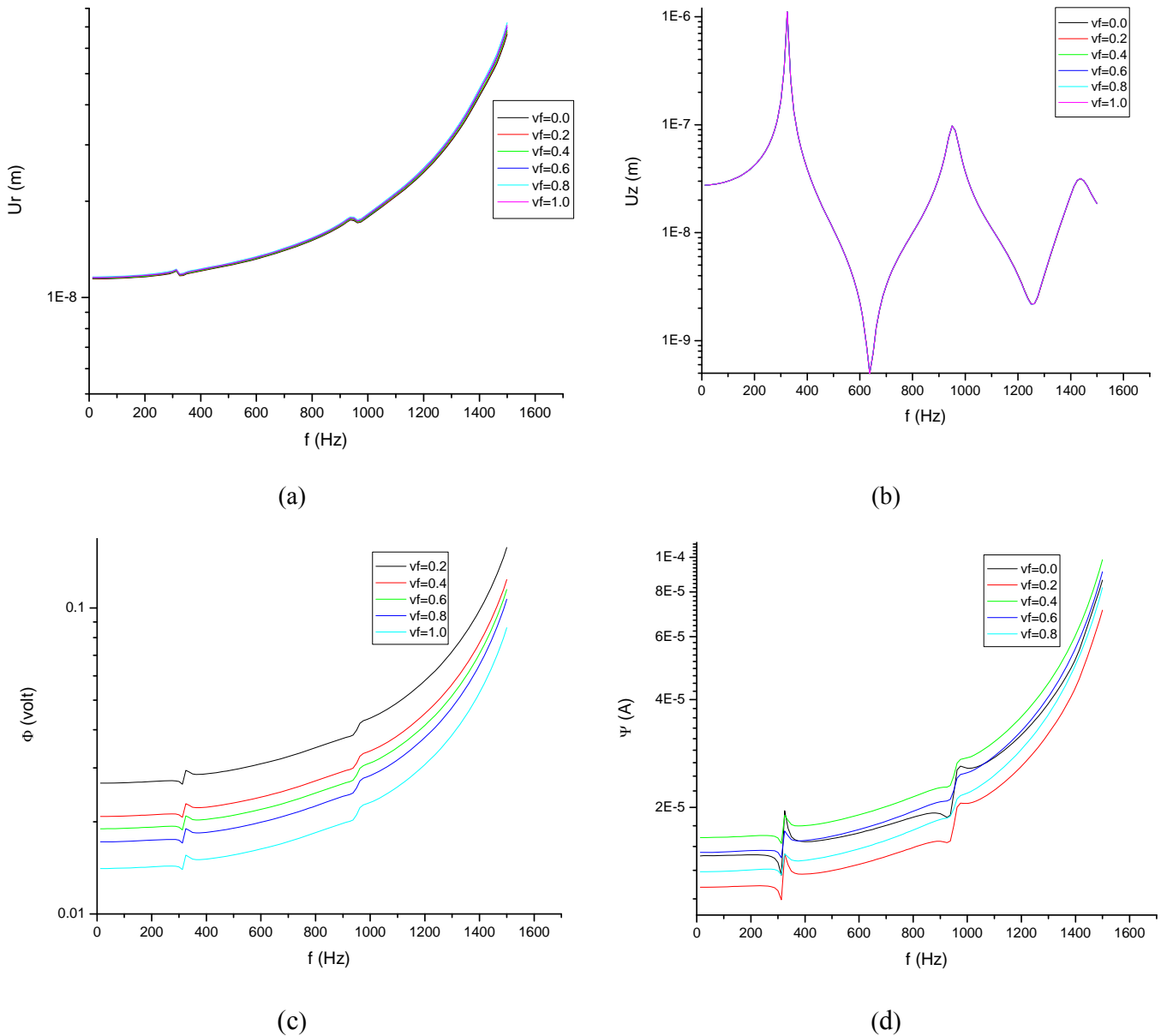


Fig. 5. (a) Radial displacement (u_r); (b) axial displacement (u_z); (c) electric potential (ϕ); and (d) magnetic potential (ψ) when sensor at free end.

3.3. Clamped-clamped Boundary Condition of the Shell

3.3.1. Sensor at Clamped End

The radial displacement (u_r), axial displacement (u_z), electric potential (ϕ) and magnetic potential (ψ) of a node on the sensor when sensor is placed at the clamped end is plotted in Fig. 6. The response is marginal for first mode of vibration where as it peaks high during second and third mode. The effect of volume fraction on magnetic response is clearly visible when the sensor is located at the clamped end with clamped-clamped boundary condition.

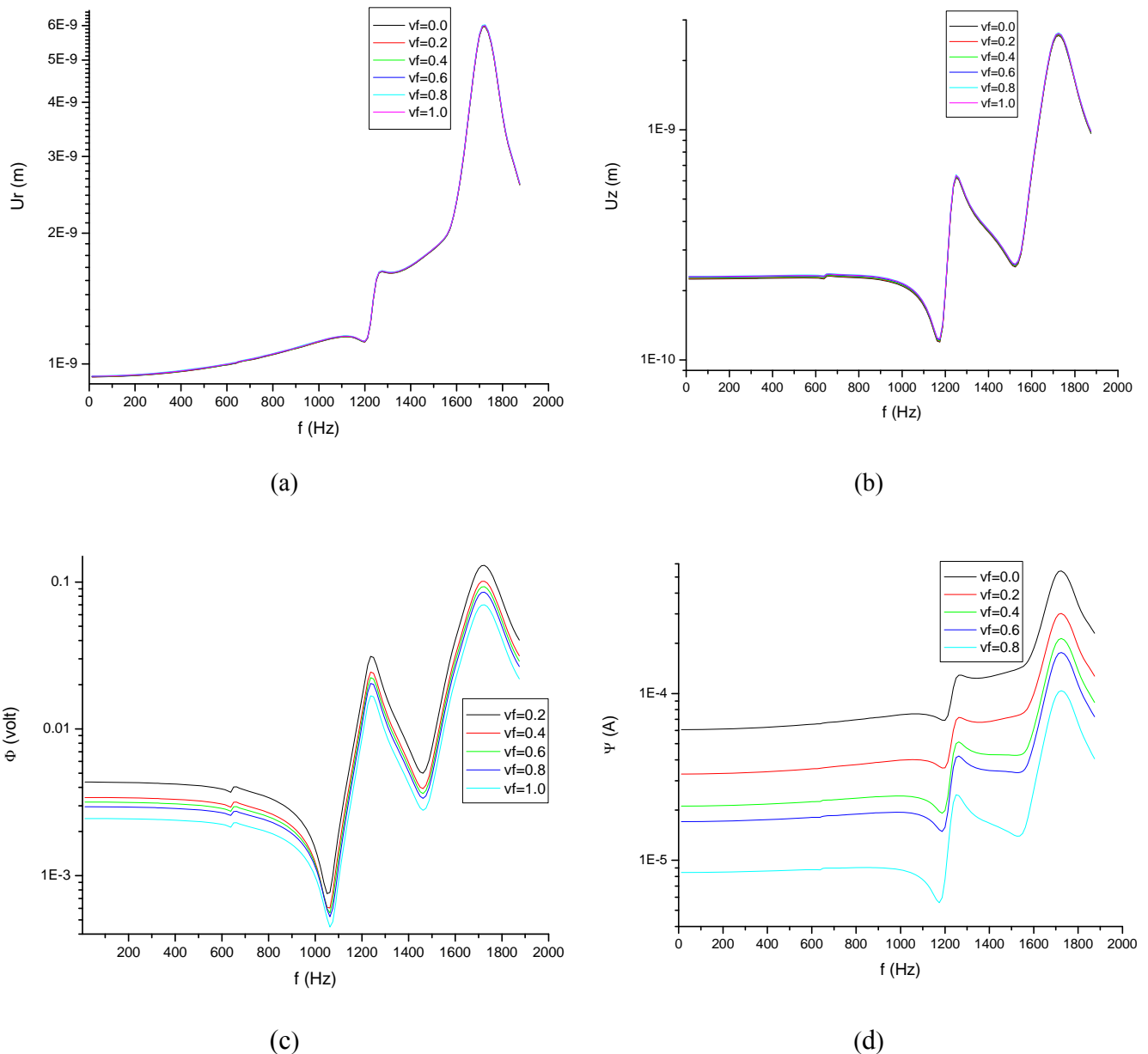


Fig. 6. (a) Radial displacement (u_r); (b) axial displacement (u_z); (c) electric potential (ϕ); and (d) magnetic potential (ψ) when sensor at clamped end.

3.3.2. Sensor at Middle

Fig. 7 shows the radial displacement (u_r), axial displacement (u_z), electric potential (ϕ) and magnetic potential (ψ) when sensor is placed at the middle of the shell. The radial displacement is seen maximum during the third mode. The electric and magnetic response follows the same pattern of radial displacement. It is unlikely to see that when $vf=0.4$ the magnetic potential (ψ) is found maximum.

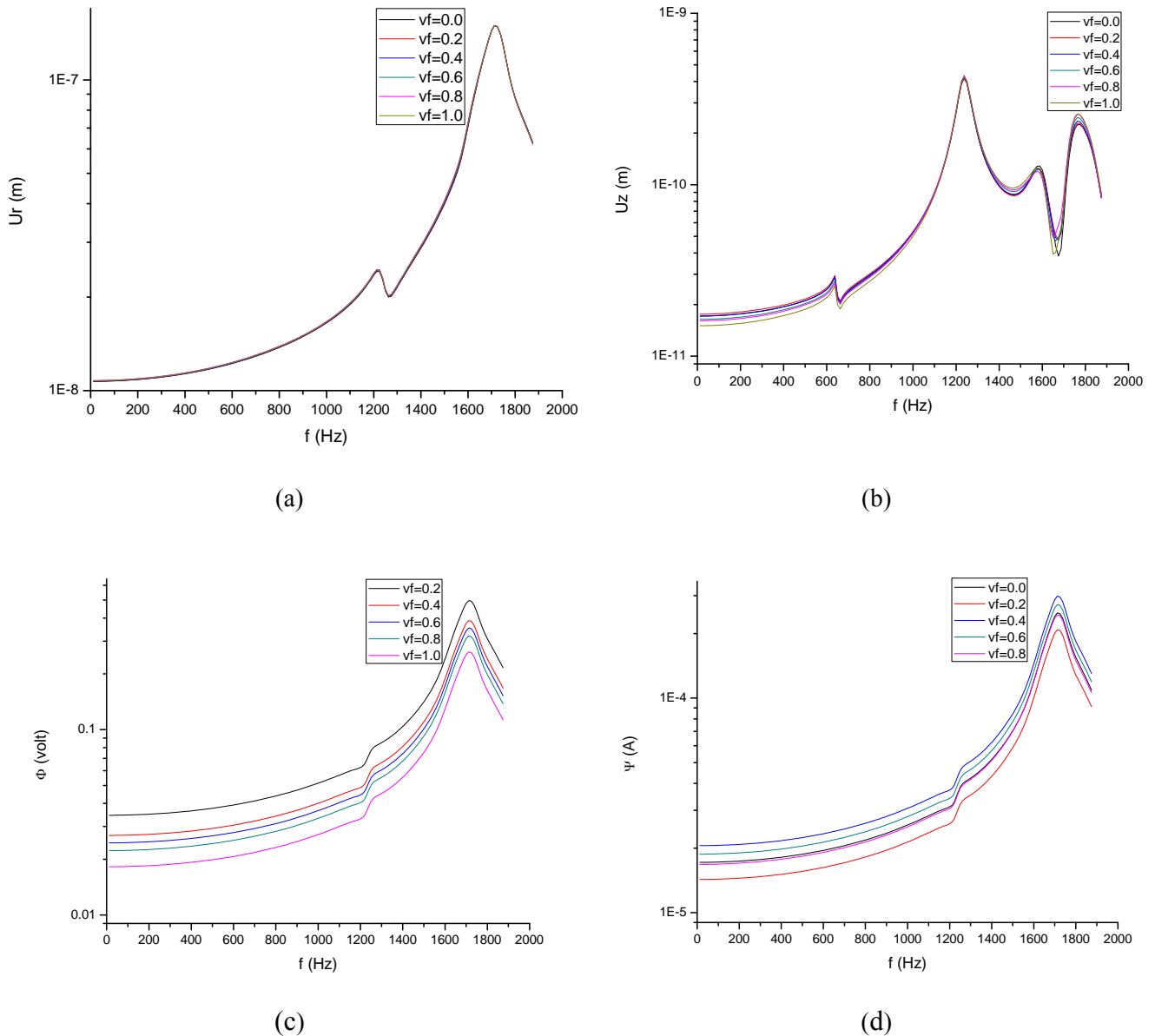


Fig. 7. (a) Radial displacement (u_r); (b) axial displacement (u_z); (c) electric potential (ϕ); and (d) magnetic potential (ψ) when sensor at middle.

4. Conclusions

Harmonic response of magneto-electro-elastic sensor bonded to a cylindrical shell is evaluated using semi analytical finite element method. The electric and magnetic response of the sensor for various sensor locations and boundary conditions are studied. The sensor response is controlled mainly by its radial displacement in all the modes. It is seen that the sensor response is maximum during the first mode when the sensor is placed at the clamped end and middle of the mild steel cylinder for clamped free boundary condition. The third mode response becomes significant when the sensor is placed at the free end for clamped free boundary condition. For clamped-clamped boundary condition the third mode response is significant for both the sensor locations.

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Guide for Contributors

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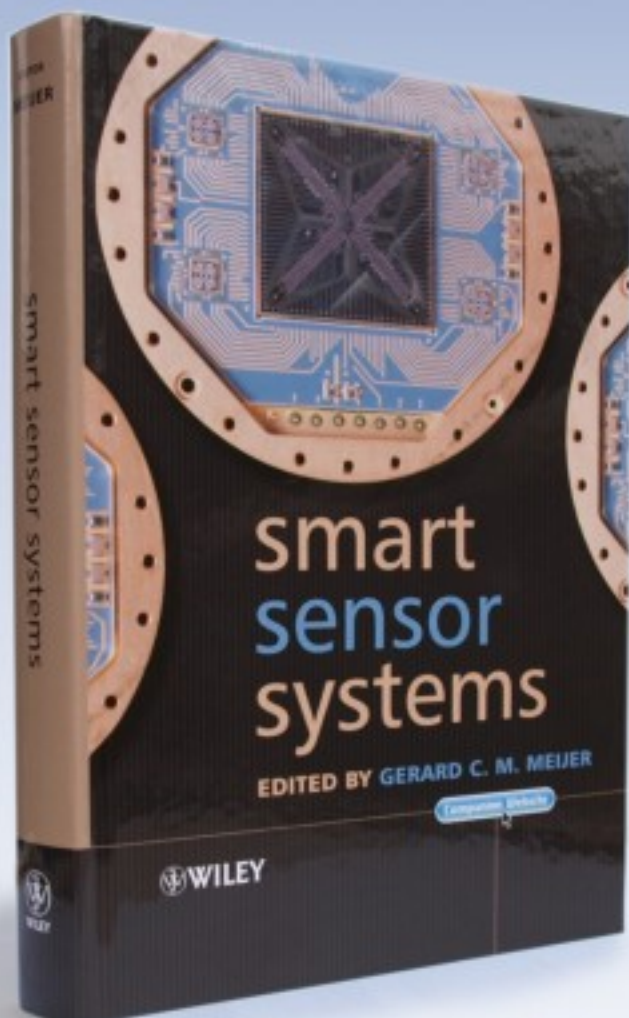
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