

State Estimation for Sensor Monitoring System with Uncertainty and Disturbance

¹ Jianhong Sun, ² Xiaoying Yu, ² Jiangwei Qiu, ³ Pengfei Guo

¹ School of Electronic Engineering and Optoelectronic Techniques, Nanjing University
of Science and Technology, Nanjing, 210094, China

² Changjiangrunfa Machinery Co., Ltd., Suzhou, 215633, China

³ School of Automation, Nanjing University of Science and Technology, Nanjing, 210094, China

¹ Tel.: +86-025-84303086

¹ E-mail: sunjh@njjust.edu.cn

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Abstract: This paper considers the state estimation problem for the sensor monitoring system which contains system uncertainty and nonlinear disturbance. In the sensor monitoring system, states of each inner sensor node usually contains system uncertainty, and external noise often works as nonlinear item. Besides, information transmission in the system is also time consuming. All mentioned above may arouse in unstable of the monitoring system. In this case, states of sensors could be wrongly sampled. Under this circumstance, a proper mathematical model is proposed and by the use of Lipschitz condition, the nonlinear item is transformed to linear one. In addition, we suppose that all sensor nodes are distributed arranged, no interface occurs with each other. By establishing proper Lyapunov–Krasovskii functional, sufficient conditions are acquired by solving linear matrix inequality to make the error augmented system stable, and the gains of observers are also derived. Finally, an illustrated example is given to show that system observed value tracks system states well, which fully demonstrate the effectiveness of our result. *Copyright © 2014 IFSA Publishing, S. L.*

Keywords: State estimation, Sensor monitoring system, System uncertainty, Nonlinear disturbance, Linear matrix inequality.

1. Introduction

During last decades, states estimation and other related problems are hot issues in the scholar field due to the increasing demand of sensor monitoring system, which is a distributed system composed of sensor nodes [1-3]. Because of its convenience for use and low cost, sensor monitoring system aroused much attention both from theoretical researches and practical occasions, such as in industry, agriculture, military and some other occasions [4]. Sensors collect data from the field and also control the operating parameters. By running a dedicated data collection procedure to achieve field data collection,

in addition, control operating parameters are transferred to sensors via data bus to achieve automatic control. However, many problems are resulted in for its special system structure. Information flow between sensor nodes is time consuming, which reflects as time-delay in system model. In addition, outer environment, take temperature, pressure, moist for example, can greatly affect sensors' working condition, so system uncertainties and disturbances are inevitable when modeling for sensor monitoring system. Take all mentioned above, states estimation is quite important for the stability analysis of sensor monitoring system.

Still now, great effort has been done to deal with states estimation problem [5-7]. Reference [8] studied the spread of subsurface contaminants, proposed a dual estimation strategy for data assimilation into a one-way coupled system by treating the flow and the contaminant models separately. This strategy didn't only deals with states estimation, but also could be used for parameter estimation. Reference [9] considered a fuzzy-integral model of a fuzzy process. Sufficient conditions were established for the existence of an optimal estimating fuzzy process. Reference [10] researched estimation problem around human environment. A Human motion map was proposed which incorporating human states information into results of conventional SLAM.

Motivated by previous research stated above, our target is to make state estimation for sensor monitoring system, which contains uncertainty and nonlinear disturbance. By establishing proper Lyapunov-Krasovskii functional, sufficient conditions are proposed to make system stable, and observe gains are also acquired.

2. Problem Formulation

Consider a type of sensor monitoring system, which is composed of several sensor nodes, and the dynamic system with uncertainty and disturbance can be described as shown in (1):

$$\begin{cases} x_i(k+1) = (A + \Delta A)x_i(k) \\ \quad + A_d x_i(k - \tau) \\ \quad + Bu(k) + E_g g(x_i(k)), \\ y_i(k) = Cx_i(k) \end{cases} \quad (1)$$

where $x_i(k) \in R^n$ denotes the state of i^{th} node, $x_i(k - \tau) \in R^n$ denotes the state delay of the node, $g(x_i(k)) \in R^n$ denotes the nonlinear disturbance, $u(k) \in R^{n_u}$ is the system input, $y_i(k) \in R^n$ denotes system output, ΔA is internal perturbation arising from uncertain factors, A , A_d , E_g , B and C are constant matrices with appropriate dimensions.

Here we make the following assumption for system model (1).

Assumption 1.

Perturbation parameter of the model satisfies:

$$\Delta A = GD(k)H \quad (2)$$

Respectively, G and H are known constant matrix, $D(k)$ is time delay uncertain matrix, yet Lebesgue-measurable, and $D^T(k)D(k) \leq I$.

Assumption 2.

State delay has an upper bound, which satisfies $0 \leq \tau \leq d$.

Assumption 3.

System nonlinear factor $g(\cdot)$ satisfies the following Lipschitz condition:

$$\|g(x_1) - g(x_2)\| \leq \|\Sigma(x_1 - x_2)\|,$$

where Σ is the constant matrix with proper dimensions, and $g(0) = 0$.

Next, a state observer for the i^{th} node is constructed.

$$\begin{cases} \hat{x}_i(k+1) = A\hat{x}_i(k) \\ \quad + \sum_{j=1}^N k_{ij} C[x_i(k) - \hat{x}_i(k)], \\ \quad + Bu(k) + E_g g(\hat{x}_i(k)) \\ \hat{y}_i(k) = C\hat{x}_i(k) \end{cases} \quad (3)$$

where $\hat{x}_i(k)$ and $\hat{y}_i(k)$ are the observed value of $x_i(k)$ and $y_i(k)$, respectively. $K_{ij} \in R^n$ is the gain of observer to be designed.

In this case, the states error and output error are defined as:

$$\begin{cases} e_{x_i}(k) = x_i(k) - \hat{x}_i(k) \\ e_{y_i}(k) = y_i(k) - \hat{y}_i(k) \end{cases}, \quad (4)$$

where

$$\begin{aligned} e_{x_i}(k+1) &= (A - \sum_{j=1}^N k_{ij} C)e_i(k) \\ &\quad + \Delta A x_i(k) + A_d x_i(k - \tau) \\ &\quad + E_g g(e_{x_i}(k)) \end{aligned} \quad (5)$$

By utilizing the Kronecker product, the error dynamics governed by (5) can be rewritten as:

$$\begin{aligned} e(k+1) &= (\tilde{A} - K\tilde{C})e(k) \\ &\quad + \Delta \tilde{A}x(k) + \tilde{A}_d x(k - \tau) \\ &\quad + \tilde{E}_g g(e_x(k)) + \tilde{E}_f f(k), \end{aligned} \quad (6)$$

where $\tilde{A} = I_N \otimes A$, $K = (k_{ij})_{n \times n}$, $\tilde{C} = I_N \otimes C$, $\Delta \tilde{A} = I_N \otimes \Delta A$, $\tilde{A}_d = I_N \otimes A_d$, $\tilde{E}_g = I_N \otimes E_g$, $\tilde{E}_f = I_N \otimes E_f$. By employing an augmented vector $Z(k) = [x^T(k) \ e^T(k)]^T$, so we have augmented system:

$$\begin{aligned} Z(k+1) &= \bar{A}Z(k) + \Delta \bar{A}Z(k) \\ &\quad + \bar{A}_d Z(k - \tau) \\ &\quad + \bar{E}_g g(Z(k)) + \bar{E}_f f(k), \end{aligned} \quad (7)$$

where

$$\bar{A} = \begin{bmatrix} \tilde{A} & 0 \\ 0 & \tilde{A} - K\tilde{C} \end{bmatrix}, \bar{A}_d = \begin{bmatrix} \tilde{A}_d & 0 \\ \tilde{A}_d & 0 \end{bmatrix}$$

$$\Delta\bar{A} = \begin{bmatrix} \Delta\tilde{A} & 0 \\ \Delta\tilde{A} & 0 \end{bmatrix}, \bar{E}_g = \begin{bmatrix} \tilde{E}_g & 0 \\ 0 & \tilde{E}_g \end{bmatrix}$$

$$\bar{E}_f = \begin{bmatrix} \tilde{E}_f \\ \tilde{E}_f \end{bmatrix}$$

Furthermore, some important lemmas will be used in this paper are listed below.

Lemma 1. For any $x, y \in R^n$, $\mu > 0$, the following equation holds.

$$2x^T y \leq \mu x^T x + \frac{1}{\mu} y^T y$$

Lemma 2. Let $Y = Y^T$, M , N , and $D(t)$ be real matrix of proper dimensions, and $D^T(t)D(t) \leq I$, then inequality $Y + MDN + (MDN)^T < 0$ holds if there exists a constant ε , which makes the following inequality holds.

$$Y + \varepsilon NN^T + \varepsilon^{-1} M^T M < 0$$

3. Main Results

In this part, two sufficient conditions are proposed to make augmented system (7) stable, in addition, the gains of observer can also be acquired.

Theorem 1. For the augmented system as shown in (7), it is said to be asymptotically stable if there exists positive definite matrix $P = \text{diag}\{P_1, P_2\}$, Q and a constant ε , make the following inequality holds.

$$\begin{bmatrix} \Omega & 0 & \Gamma & 0 & 0 & 0 \\ * & -Q & 0 & 0 & 2\bar{A}_d^T P & 0 \\ * & * & -P & 0 & 0 & 0 \\ * & * & * & -P & 0 & \tilde{G}^T \bar{P} \\ * & * & * & * & -P & 0 \\ * & * & * & * & * & -\varepsilon I \end{bmatrix} < 0$$

where

$$\Omega = -P + (1+d)Q + 4\lambda \Sigma^T \Sigma + \varepsilon \bar{H}^T \bar{H}$$

$$\bar{H} = [\tilde{H} \quad 0]$$

$$\bar{P} = [P_1^T \quad P_2^T]^T$$

$$\tilde{G} = I_N \otimes G$$

Proof: By constructing the following Lyapunov-Krasovskii functional

$$V(k) = V_1(k) + V_2(k), \quad (8)$$

where

$$V_1(k) = Z^T(k) P Z(k)$$

$$V_2(k) = \sum_{i=k-\tau}^{k-1} Z^T(i) Q Z(i) + \sum_{j=1-d}^0 \sum_{i=k+j}^{k-1} Z^T(i) Q Z(i)$$

So the forward difference of $V(k)$ along (7) is:

$$\begin{aligned} & E\Delta V_1 \\ &= E\{Z^T(k+1)PZ(k+1) \\ &\quad - Z^T(k)PZ(k)\} \\ &= Z^T(k)\bar{A}^T P \bar{A} Z(k) \\ &\quad + 2Z^T(k)\bar{A}^T P \Delta \bar{A} Z(k) \\ &\quad + 2Z^T(k)\bar{A}^T P \bar{A}_d Z(k-\tau) \\ &\quad + 2Z^T(k)\bar{A}^T P \bar{E}_g g(Z(k)) \\ &\quad + Z^T(k)\Delta \bar{A}^T P \Delta \bar{A} Z(k) \\ &\quad + 2Z^T(k)\Delta \bar{A}^T P \bar{A}_d Z(k-\tau) \\ &\quad + 2Z^T(k)\Delta \bar{A}^T P \bar{E}_g g(Z(k)) \\ &\quad + Z^T(k-\tau)\bar{A}_d^T P \bar{A}_d Z(k-\tau) \\ &\quad + 2Z^T(k-\tau)\bar{A}_d^T P \bar{E}_g g(Z(k)) \\ &\quad + g^T(Z(k))\bar{E}_g^T P \bar{E}_g g(Z(k)) \\ &\quad - Z^T(k)PZ(k) \end{aligned} \quad (9)$$

By the use of **Lemma 1**, we can obtain:

$$\begin{aligned} & 2Z^T(k)\bar{A}^T P \bar{A}_d Z(k-\tau) \\ & \leq Z^T(k)\bar{A}^T P \bar{A} Z(k) \\ & \quad + Z^T(k-\tau)\bar{A}_d^T P \bar{A}_d Z(k-\tau) \end{aligned} \quad (10)$$

$$\begin{aligned} & 2Z^T(k)\bar{A}^T P \bar{A}_d Z(k-\tau) \\ & \leq Z^T(k)\bar{A}^T P \bar{A} Z(k) \\ & \quad + Z^T(k-\tau)\bar{A}_d^T P \bar{A}_d Z(k-\tau) \end{aligned} \quad (11)$$

$$\begin{aligned} & 2Z^T(k)\bar{A}^T P \bar{E}_g g(Z(k)) \\ & \leq Z^T(k)\bar{A}^T P \bar{A} Z(k) \\ & \quad + g^T(Z(k))\bar{E}_g^T P \bar{E}_g g(Z(k)) \end{aligned} \quad (12)$$

$$\begin{aligned} & 2Z^T(k)\Delta\bar{A}^T P\bar{A}_d Z(k-\tau) \\ & \leq Z^T(k)\Delta\bar{A}^T P\Delta\bar{A}Z(k) \\ & \quad + Z^T(k-\tau)\bar{A}_d^T P\bar{A}_d Z(k-\tau) \end{aligned} \quad (13)$$

$$\begin{aligned} & 2Z^T(k)\Delta\bar{A}^T P\bar{E}_g g(Z(k)) \\ & \leq Z^T(k)\Delta\bar{A}^T P\Delta\bar{A}Z(k) \\ & \quad + g^T(Z(k))\bar{E}_g^T P\bar{E}_g g(Z(k)) \end{aligned} \quad (14)$$

$$\begin{aligned} & 2Z^T(k-\tau)\bar{A}_d^T P\bar{E}_g g(Z(k)) \\ & \leq Z^T(k-\tau)\bar{A}_d^T P\bar{A}_d Z(k-\tau) \\ & \quad + g^T(Z(k))\bar{E}_g^T P\bar{E}_g g(Z(k)) \end{aligned} \quad (15)$$

According to assumption 3, nonlinear disturbance can be rewritten into the form:

$$\begin{aligned} & g^T(Z(k))\bar{E}_g^T P\bar{E}_g g(Z(k)) \\ & \leq \lambda_{\max}(\bar{E}_g^T P\bar{E}_g) g^T(Z(k))g(Z(k)) \\ & \leq \lambda Z^T(k)\Sigma^T \Sigma Z(k) \end{aligned} \quad (16)$$

$$\begin{aligned} & E\Delta V_2 \\ & = \sum_{i=k+1-\tau}^k Z^T(i)QZ(i) - \sum_{i=k-\tau}^{k-1} Z^T(i)QZ(i) \\ & \quad + \sum_{j=1-d}^0 \sum_{i=k+1+j}^k Z^T(i)QZ(i) \\ & \quad - \sum_{j=1-d}^0 \sum_{i=k+j}^{k-1} Z^T(i)QZ(i) \\ & \leq Z^T(k)QZ(k) - Z^T(k-\tau)QZ(k-\tau) \\ & \quad + \sum_{i=k+1-\tau}^{k-1} Z^T(i)QZ(i) \\ & \quad + \sum_{j=1-d}^0 \{Z^T(k)QZ(k) \\ & \quad - Z^T(k+j)QZ(k+j)\} \\ & = Z^T(k)QZ(k) - Z^T(k-\tau)QZ(k-\tau) \\ & \quad + \sum_{i=k+1-\tau}^k Z^T(i)QZ(i) \\ & \quad + dZ^T(k)QZ(k) - \sum_{i=k+1-\tau}^k Z^T(i)QZ(i) \\ & = (1+d)Z^T(k)QZ(k) \\ & \quad - Z^T(k-\tau)QZ(k-\tau) \end{aligned} \quad (17)$$

By substituting (9) to (17) into (8), we have:

$$\begin{aligned} E\Delta V & = E\{\Delta V_1 + \Delta V_2\} \\ & = X^T(k)YX(k) \end{aligned}$$

where

$$X(k) = \begin{bmatrix} Z^T(k) & Z^T(k-\tau) \end{bmatrix}^T$$

$$Y = \begin{bmatrix} Y_{11} & 0 \\ 0 & Y_{22} \end{bmatrix}$$

$$Y_{11} = 4\bar{A}^T P\bar{A} + 4\Delta\bar{A}^T P\Delta\bar{A} + 4\lambda \Sigma^T \Sigma - P + (1+d)Q$$

$$Y_{22} = 4\bar{A}_d^T P\bar{A}_d - Q$$

According to Schur complement, $Y < 0$ equals to:

$$\begin{bmatrix} Y_1 & 0 & 2\bar{A}^T & 2\Delta\bar{A}^T & 0 \\ * & -Q & 0 & 0 & 2\bar{A}_d^T \\ * & * & -P^{-1} & 0 & 0 \\ * & * & * & -P^{-1} & 0 \\ * & * & * & * & -P^{-1} \end{bmatrix} < 0,$$

where

$$Y_1 = -P + (1+d)Q + 4\lambda \Sigma^T \Sigma$$

Multiply $diag\{I, I, P, P, P\}$ on both sides of the inequality, the following inequality can be acquired.

$$\begin{bmatrix} Y_1 & 0 & 2\bar{A}^T P & 2\Delta\bar{A}^T P & 0 \\ * & -Q & 0 & 0 & 2\bar{A}_d^T P \\ * & * & -P & 0 & 0 \\ * & * & * & -P & 0 \\ * & * & * & * & -P \end{bmatrix} < 0 \quad (18)$$

According to Lemma 2 and the notation defined in the theorem, result can be easily acquired, so the proof of Theorem 1 is complete.

Theorem 1 only demonstrate the stability of error system (7), however, observer gains can't be acquired, so the following theorem is given.

Theorem 2. For the augmented system as shown in (7), it is said to be asymptotically stable if there exists positive definite matrix $P = diag\{P_1, P_2\}$, Q and a constant ε , make the following inequality holds.

$$\begin{bmatrix} \Omega & 0 & 2\bar{A}^T P & 0 & 0 & 0 \\ * & -Q & 0 & 0 & 2\bar{A}_d^T P & 0 \\ * & * & -P & 0 & 0 & 0 \\ * & * & * & -P & 0 & \tilde{G}^T \bar{P} \\ * & * & * & * & -P & 0 \\ * & * & * & * & * & -\varepsilon I \end{bmatrix} < 0,$$

where

$$\begin{aligned}\Omega &= -P + (1+d)Q + 4\lambda \Sigma^T \Sigma + \varepsilon \bar{H}^T \bar{H} \\ \bar{H} &= [\tilde{H} \quad 0] \\ \bar{P} &= [P_1^T \quad P_2^T]^T \\ \tilde{G} &= I_N \otimes G \\ \Gamma &= 2 \begin{bmatrix} \tilde{A}P_1 & 0 \\ 0 & \tilde{A}P_2 - \tilde{C}^T S \end{bmatrix}\end{aligned}$$

Ω , \bar{H} , \bar{P} , \tilde{G} have the same meaning as defined in Theorem 1, and the gain of observe is:

$$K = P_2^{-1} S^T$$

Proof: Setting $K^T P_2 = S$, so $K = P_2^{-1} S^T$, by substituting $K^T P_2 = S$ into Theorem 1, we can get the result easily.

4. Numerical Example

In this part, a numerical example is given to show the effectiveness of proposed method. Transform the case on [11], parameters in (1) are given as:

$$\begin{aligned}A &= \begin{bmatrix} 0.2546 & 0.2472 \\ 0.2323 & 0.2268 \end{bmatrix}, \\ A_d &= \begin{bmatrix} -0.1434 & 0.0061 \\ -0.0118 & 0.0384 \end{bmatrix}, B = \begin{bmatrix} 0.1669 \\ 0.1174 \end{bmatrix}, \\ E_g &= \begin{bmatrix} -0.0130 \\ 0.0742 \end{bmatrix}, \\ C &= \begin{bmatrix} 1.1866 & 0.4552 \\ 0.5395 & 0.3164 \end{bmatrix}, \\ G &= \begin{bmatrix} 0.0618 & 0.1236 \\ 0 & 0.1422 \end{bmatrix}, \\ D(k) &= \begin{bmatrix} 0.2\sin(0.6k) & 0 \\ 0 & 0.2\sin(0.6k) \end{bmatrix}, \\ H &= \begin{bmatrix} 0.4450 & 0.3214 \\ 0.2596 & -0.4326 \end{bmatrix}, \\ g_i(x(k)) &= [0.12 \cos x_{i1}(k) \quad 0.41x_{i2}]^T \\ u(k) &= 5e^{-0.01k} \sin(k)\end{aligned}$$

The initial states of each sensor nodes are:

$$x_1 = \begin{bmatrix} 3.2 \\ -3.5 \end{bmatrix}, x_2 = \begin{bmatrix} 2.2 \\ -1.6 \end{bmatrix}, x_3 = \begin{bmatrix} 2.72 \\ 3.25 \end{bmatrix}$$

Observer gain can be obtained based on Theorem 1 and Theorem 2, we have:

$$k_{11} = k_{22} = k_{33} = \begin{bmatrix} -0.4067 & 1.3663 \\ -0.3762 & 1.2581 \end{bmatrix}$$

Simulation results are given in Fig. 1, where red lines denotes for real system state, blue dashed line denotes for observed value. From the result, we can see that observed value tracks system states well, which can fully demonstrate the effectiveness of proposed method. Estimation error is shown in Fig. 2, which is much smaller than the method proposed in [12], compared with Fig. 3.

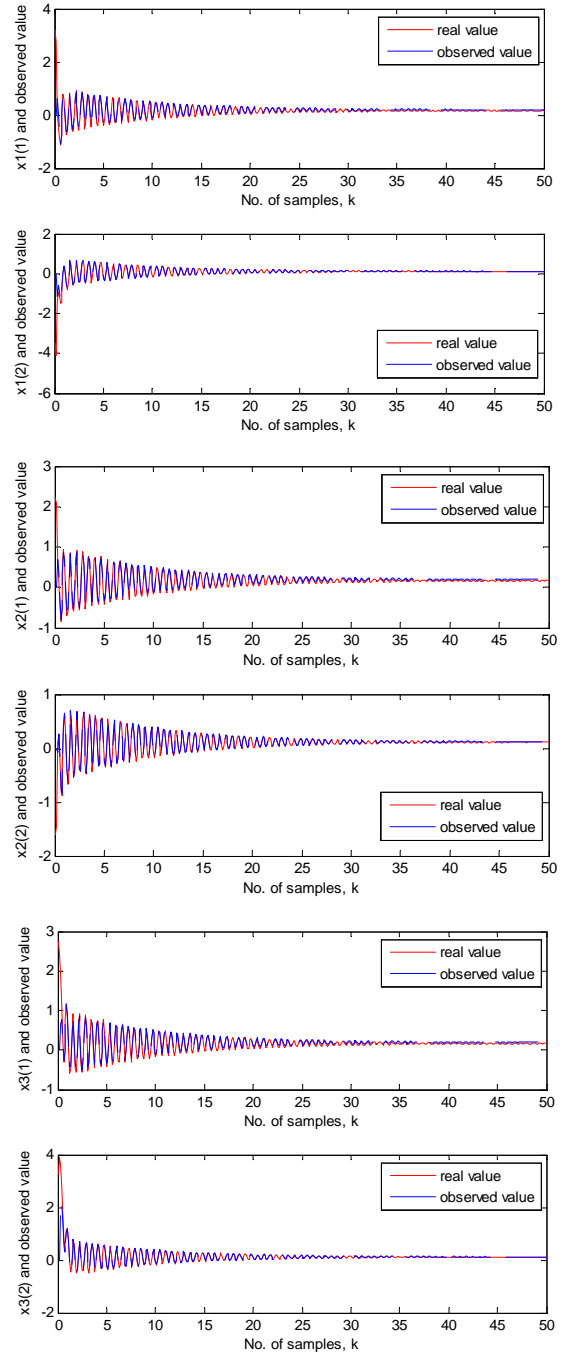
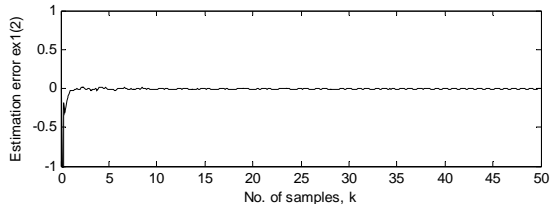
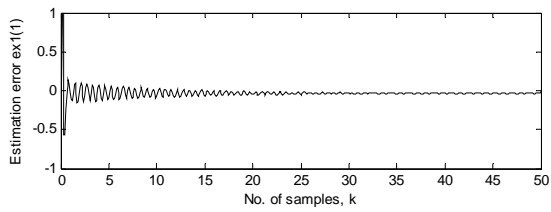
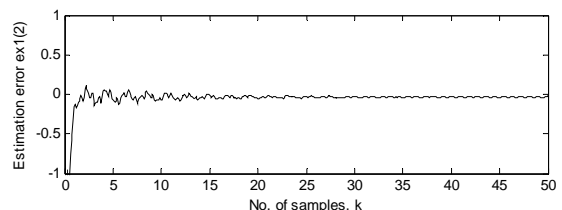
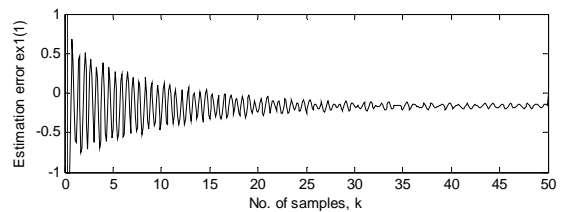


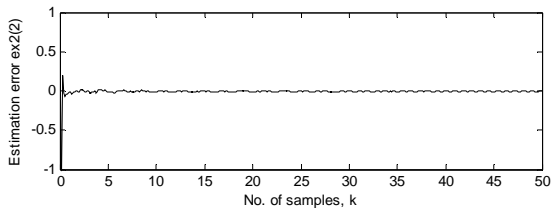
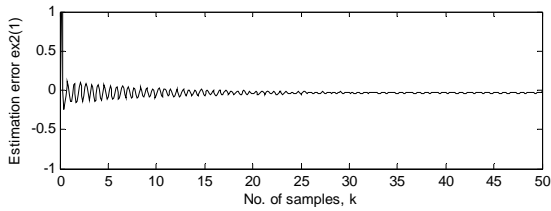
Fig. 1. System states and observed value.



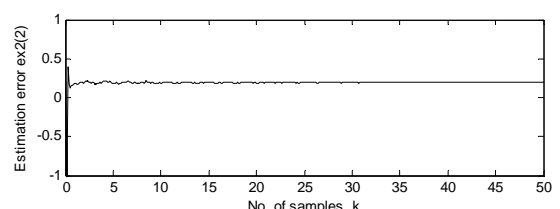
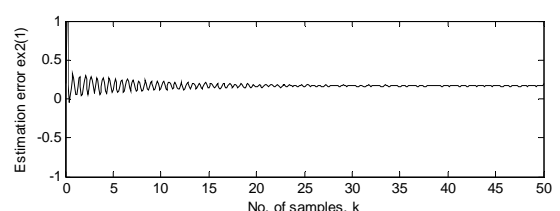
(a) Estimation error e_{x1}



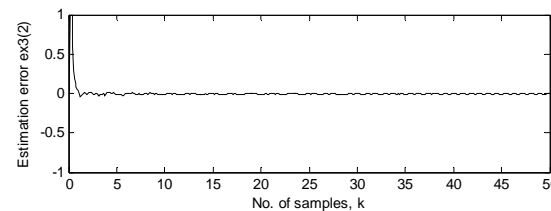
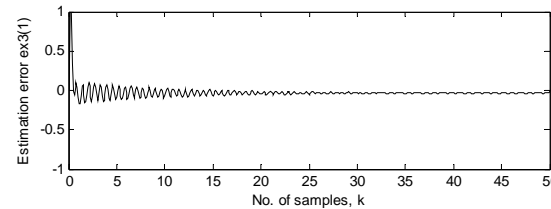
(a) Estimation error e_{x1}



(b) Estimation error e_{x2}

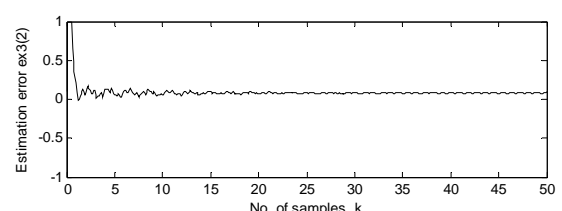
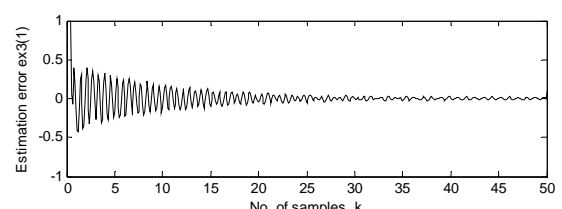


(b) Estimation error e_{x2}



(c) Estimation error e_{x3}

Fig. 2. Estimation error for system states.



(c) Estimation error e_{x3}

Fig. 3. Method proposed in [12].

5. Conclusions

This paper deals with the state estimation problem for a class of sensor monitoring system, which contains system uncertainty and nonlinear disturbance. By establishing proper Lyapunov–Krasovskii functional, sufficient conditions are proposed to guarantee the stability of error system, and the gains of observes are also acquired. Finally, an illustrated example shows the effectiveness of proposed method.

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Universal Sensors and Transducers Interface (USTI)

for any sensors and transducers with frequency, period, duty-cycle, time interval, PWM, phase-shift, pulse number output



The image shows a large blue USTI chip with gold pins, and two smaller versions of the same chip. To the left of the chips are several white icons representing different sensor types: a square wave, a variable resistor, a variable capacitor, a Wheatstone bridge, and a gear.

- * Input frequency range: 0.05 Hz ... 9 MHz (144 MHz)
- * Selectable and constant relative error: 1 ... 0.0005 % for all frequency range
- * Scalable resolution
- * Non-redundant conversion time
- * RS232, SPI, I2C interfaces
- * Rotational speed, *rpm*
- * Cx, 50 pF to 100 μF
- * Rx, 10 Ω to 10 MΩ
- * Pt100, Pt1000, Pt5000, Cu, Ni
- * Resistive Bridges
- * PDIP, TQFP, MLF packages

Just make it easy !

<http://www.techassist2010.com/> info@techassist2010.com